

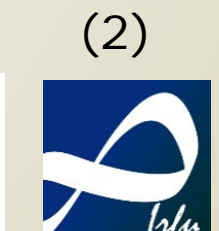
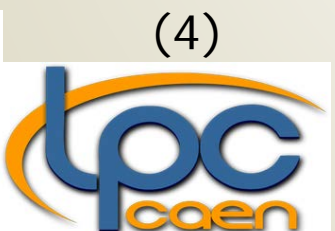


# INTERNATIONAL CONFERENCE ON ION SOURCES



## ASTERICS, A NEW SUPERCONDUCTING ECRIS FOR SPIRAL2

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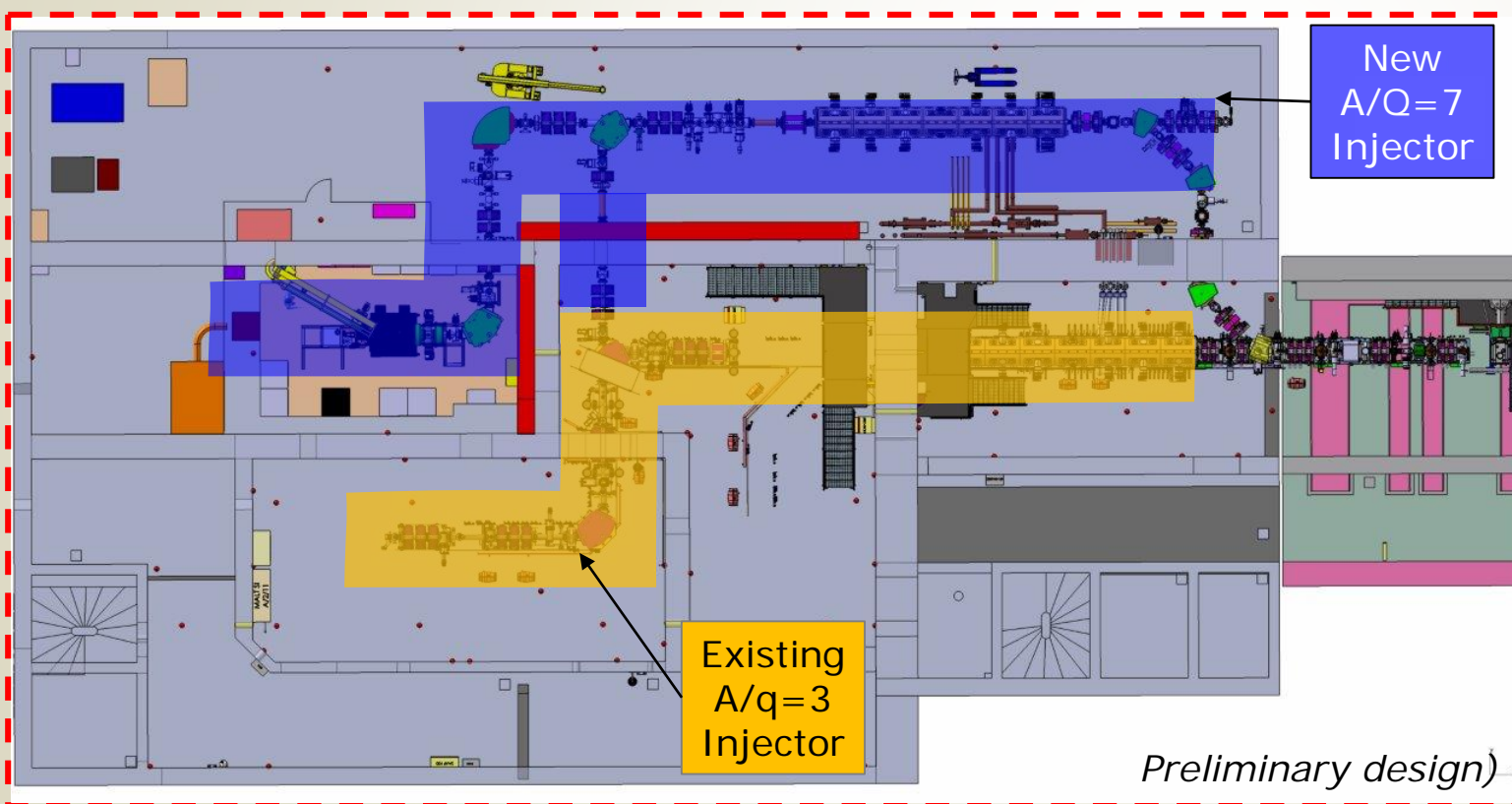


# OUTLINE

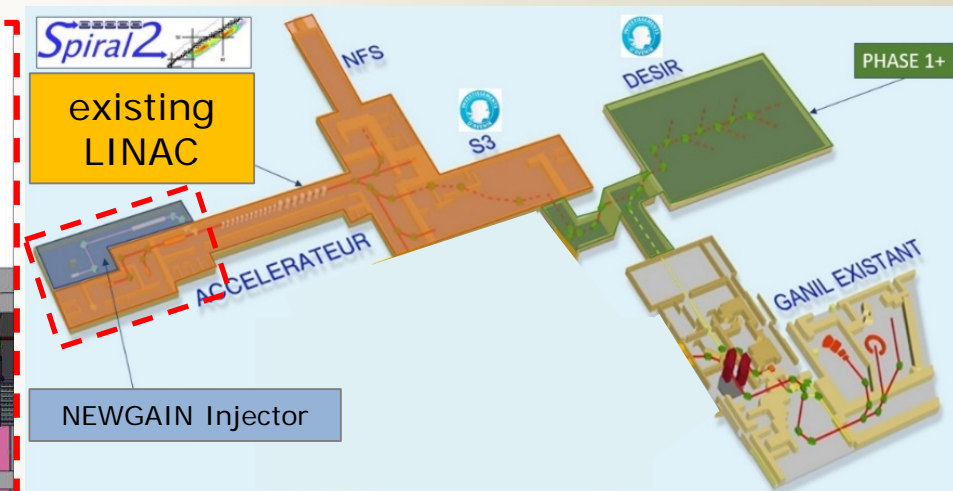
- NEWGAIN project, beam requirements and how to answer them
- Motivation to build a large ECR 28 GHz ECRIS
- Status of the ASTERICS design
- Concept of thick active hot liner for metallic beam operation

# NEWGAIN: NEW GANIL INjector

- Funded Project to design and build a  $M/Q=7$  heavy ion injector for the SPIRAL2 accelerator at GANIL, Caen , France
- French multi-laboratory collaboration
- Project Timeline : 2023-2030



*Preliminary design)*



**NEWGAIN**  
NEW GANIL INJECTOR



# NEWGAIN Ion Source Specifications

## Project Specifications

- RFQ input: 10 kV/Q with  $M/Q \leq 7$
- Single charge state ion beam
- Accelerate heavy ions up to uranium
  - 13  $\mu\text{A}$  for  $M \leq 100$
  - 10  $\mu\text{A}$  for  $M > 100$
- Minimize the project risk (SC magnet)

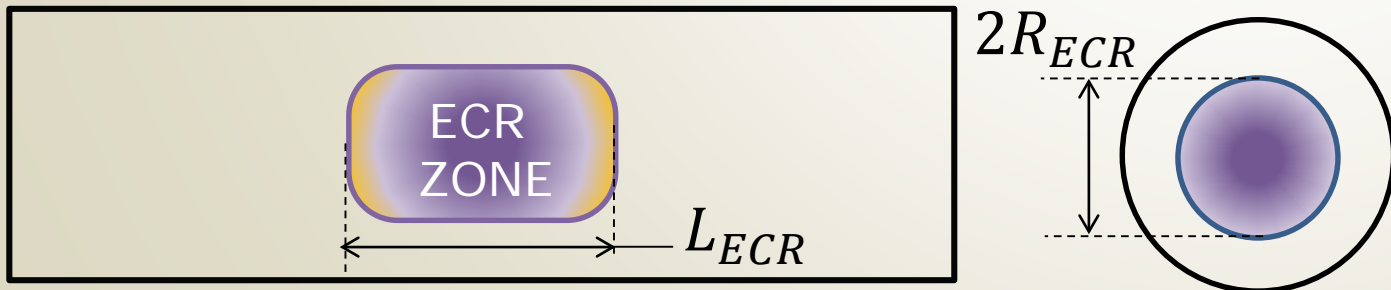
## Discussion

- 18 GHz plasma sufficient to make the  $M \leq 100$  beam intensities
- 28 GHz ECRIS required to produce the  $M > 100$  beam intensities
- Practical state of the art 28 GHz  $\text{U}^{34+}$  intensity in operation:  $\sim 200 \mu\text{A}$  (6  $\mu\text{A}$ )
- How to produce 10  $\mu\text{A}$  of  $\text{U}^{34+}$  ?
- And keeping the project risk low?
- Can a larger volume ECR source @28 GHz answer the need?

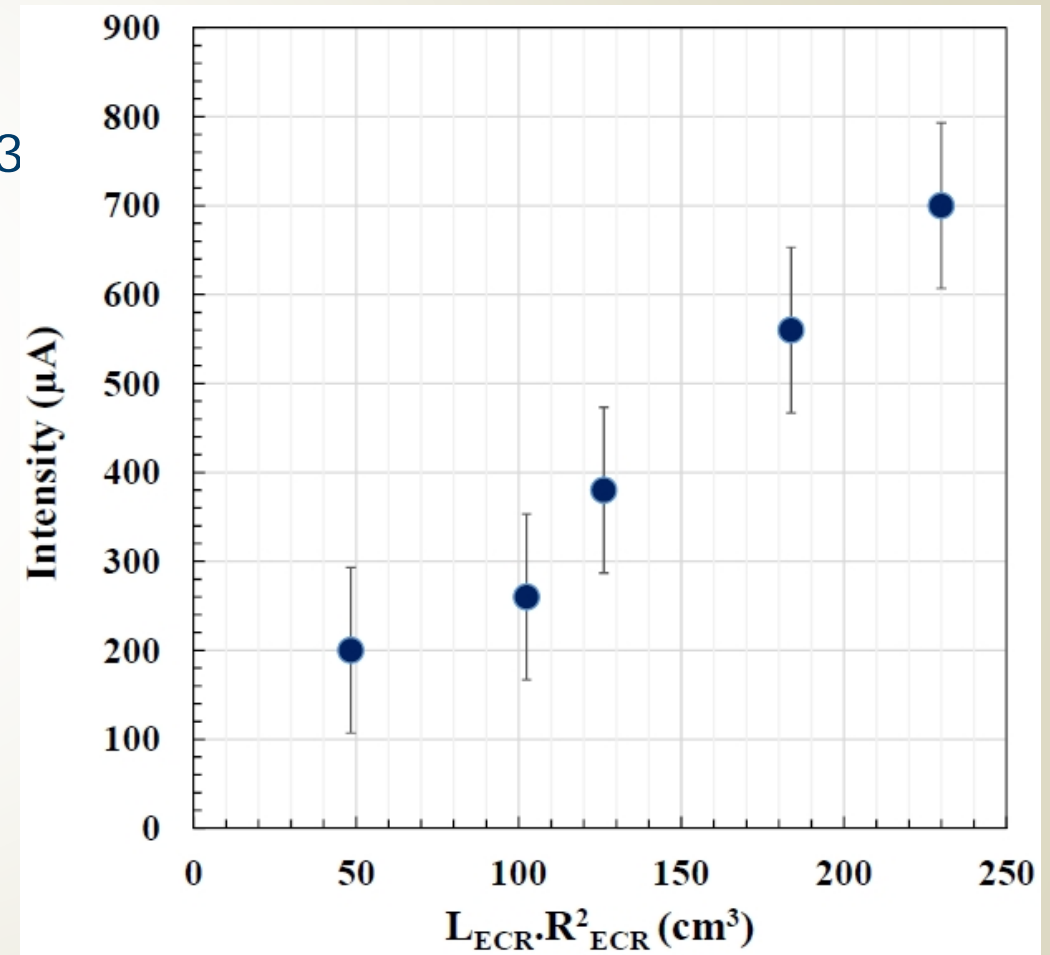


# ECR Volume and Ion beam intensity (1/2)

- Return of experience from the 18 GHz ECRIS
- Plotting  $\text{Ar}^{12+}$  Beam intensity vs  $L_{ECR} \times R_{ECR}^2 (\approx V_{ECR})$
- For several ion sources : PHOENIX V2, PHOENIX V3 GTS, HIISI, SUSI
- Magnetic structures are comparable as they follow the magnetic scaling laws
- RF Power/cm<sup>3</sup> ~ const ~ 0.5 W/cm<sup>3</sup>
- $n_e$  and  $T_e$  ~ const
- $I \approx V_{ECR}$

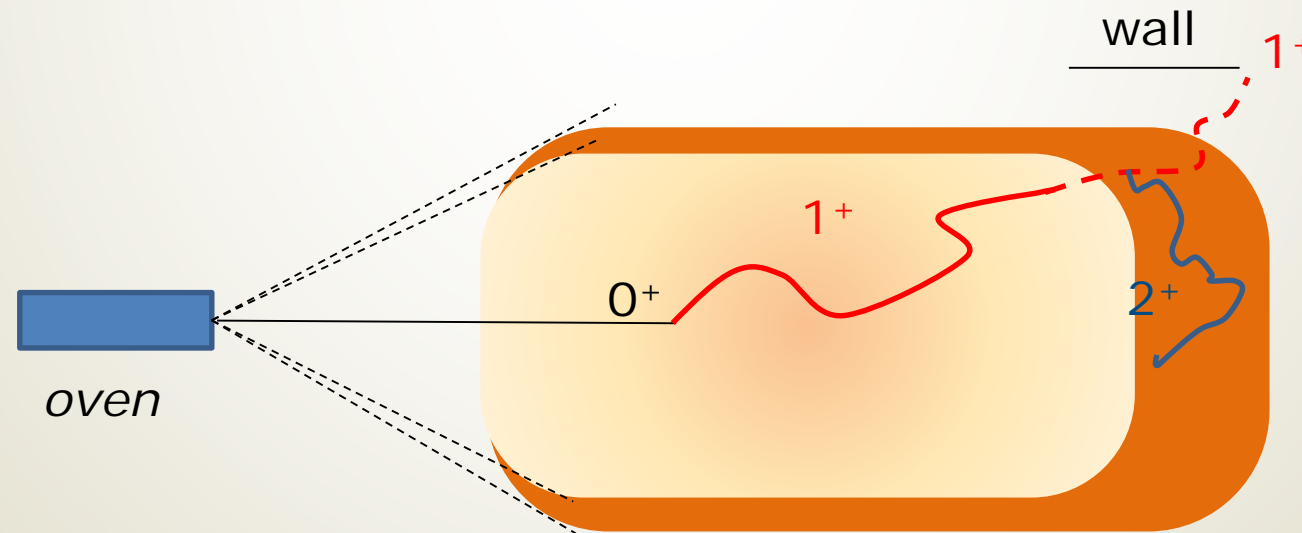


$\text{Ar}^{12+}$  Beam intensity



## ECR Volume and Ion beam intensity (2/2)

- A longer plasma will make more ion beam
- A larger plasma will boost  $U^{34+}$  intensity wrt  $U^{33+}$
- This is the strategy chosen to target 10  $\mu\text{A}$   $U^{34+}$  beam intensity
- Bonus: enhancement of metal vapor capture with a larger plasma volume



## Minimizing risks for the SC ECRI S design

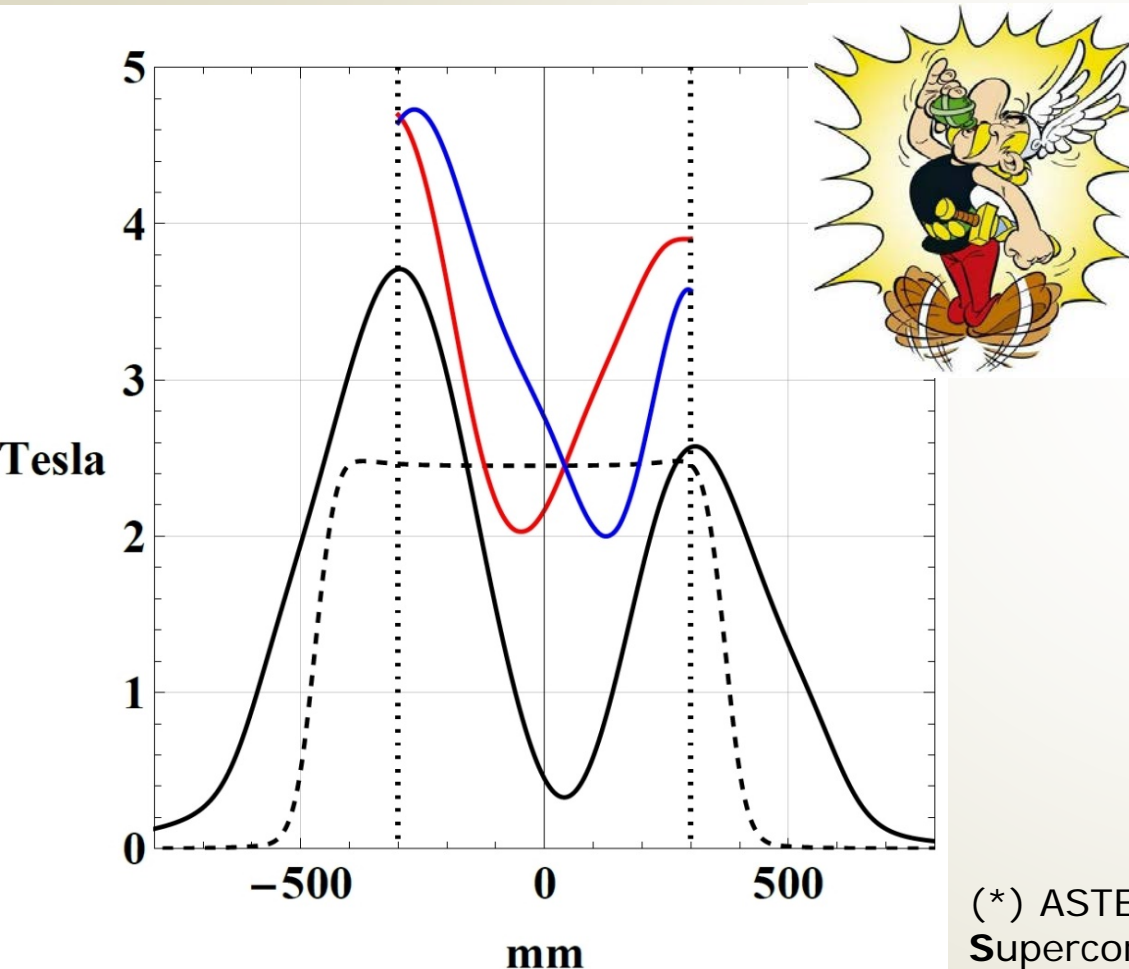
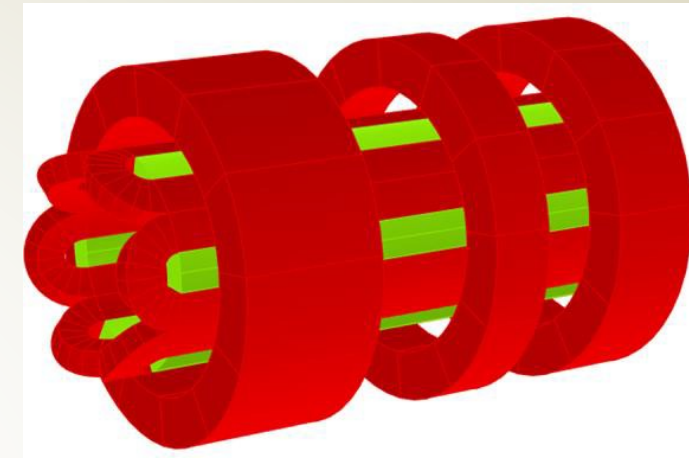
- Use the positive return of experience from VENUS, SECRAI II, RIKEN SC  
=> Choose the ECR frequency at **28 GHz**
- Use the bladder and keys technique to mitigate the risk on the hexapole coil assembly  
=> as for VENUS-FRIB and FECR
- keep the existing VENUS-FRIB magnet mechanics design system topology

## Improving beam intensities with a larger plasma volume

- Choice for ASTERICS plasma chamber : L=600 mm, r=91 mm
  - VENUS (L=500 mm, r=71 mm)
- U<sup>34+</sup> Ion beam expected  $\geq 8-9$  pμA for long run operation
  - State of the art  $\sim 6$  pμA (VENUS)

# ASTERICS\* SC magnet

- Designed by CEA Irfu
- Axial max profile 3.7-0.1-2.5 T



- Radial field  $B_r \sim 2.45 \text{ T} @ r = 91 \text{ mm}$
- Last closed magnetic surface at wall for 3.7-0.3-2.5 T is  $|\mathbf{B}| \sim 2\text{T}$
- Benefit of a larger ECR source is the relaxation of the unwanted radial component of the axial coil magnetic field
- Also relaxes forces on hexapole coils (counter-intuitive)

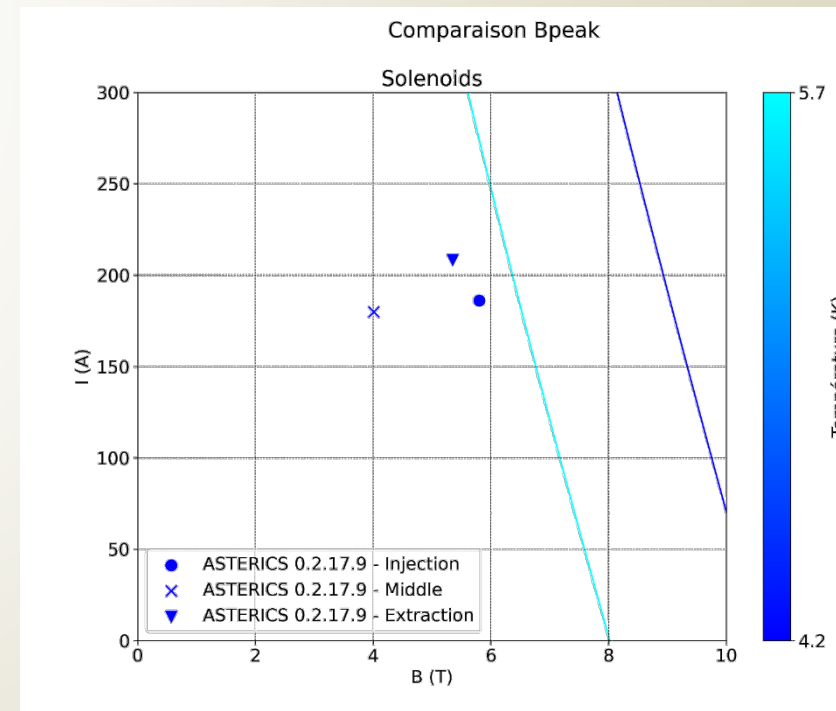
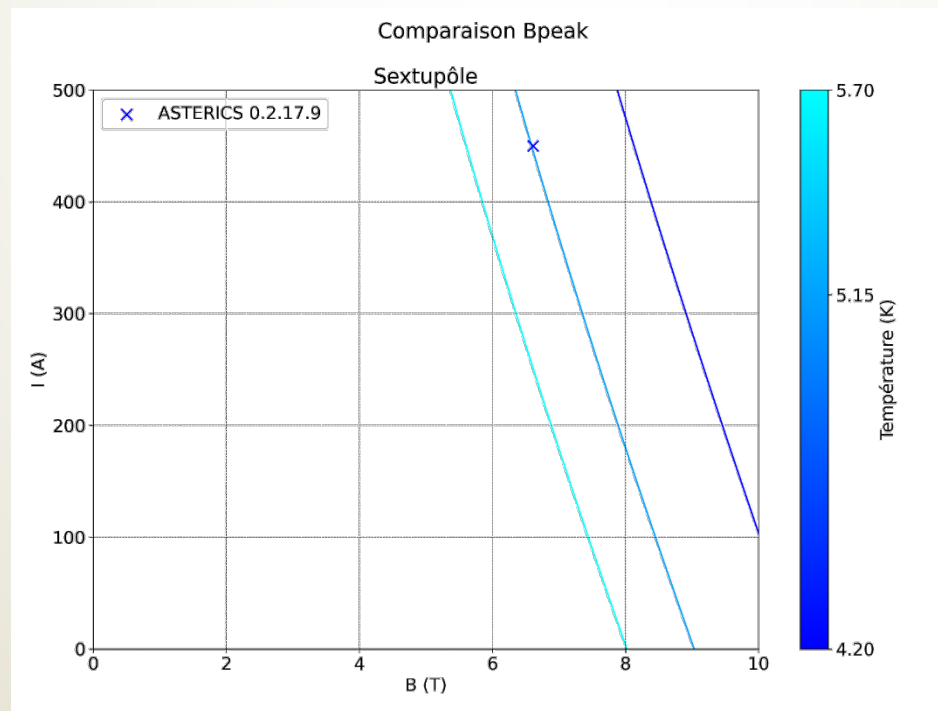
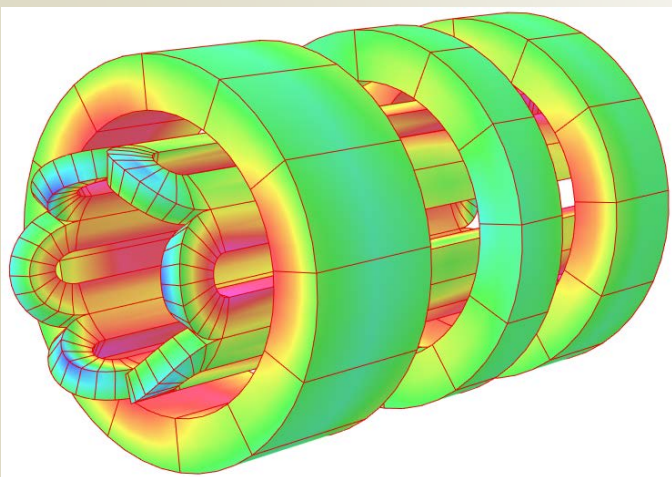
(\* ASTERICS=Advanced Spiral Two Electron cyclotron Resonance Ion source with Superconducting magnets at Caen



# ASTERICS B Peak Fields and Temperature Margin

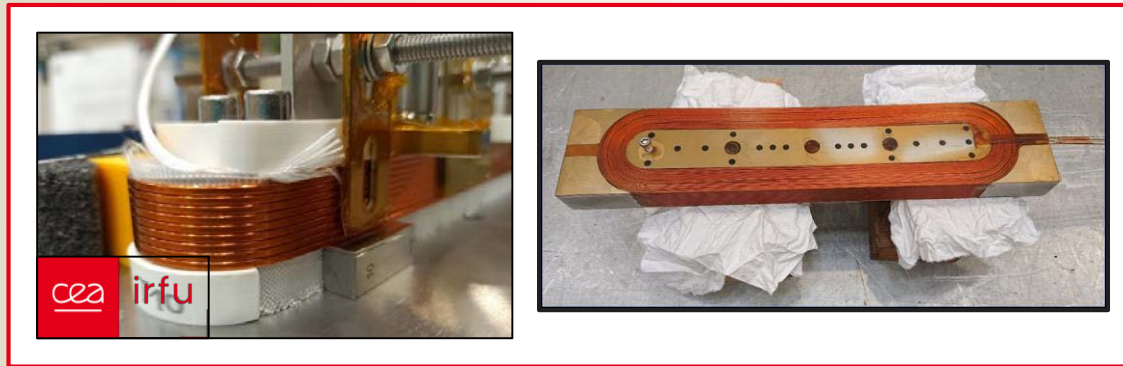
- Same conductor type as VENUS FRIB , cable recently ordered (Furukawa, JP)
- Temperature Margin:
  - > 1.5 K for solenoids
  - ~ 1 K for hexapole

	Solen. INJ			Solen. MID			Solen. EXT			hexapole		
	B Peak (T)	I (A)	T (K)	B Peak (T)	I (A)	T (K)	B Peak (T)	I (A)	T (K)	B Peak (T)	I (A)	T (K)
ASTERICS 0.2.17.9	5.8	186.1	6.04	4.01	-180	6.95	5.35	208.4	6.18	6.61	450	5.15

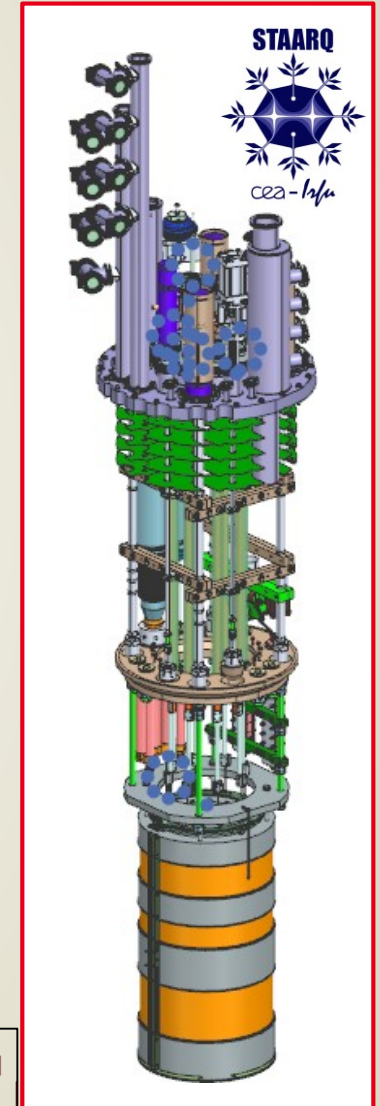


# ASTERICS magnet construction strategy

- Racetrack Mock-up recently built at CEA
  - to test the winding technique and epoxy impregnation under vacuum



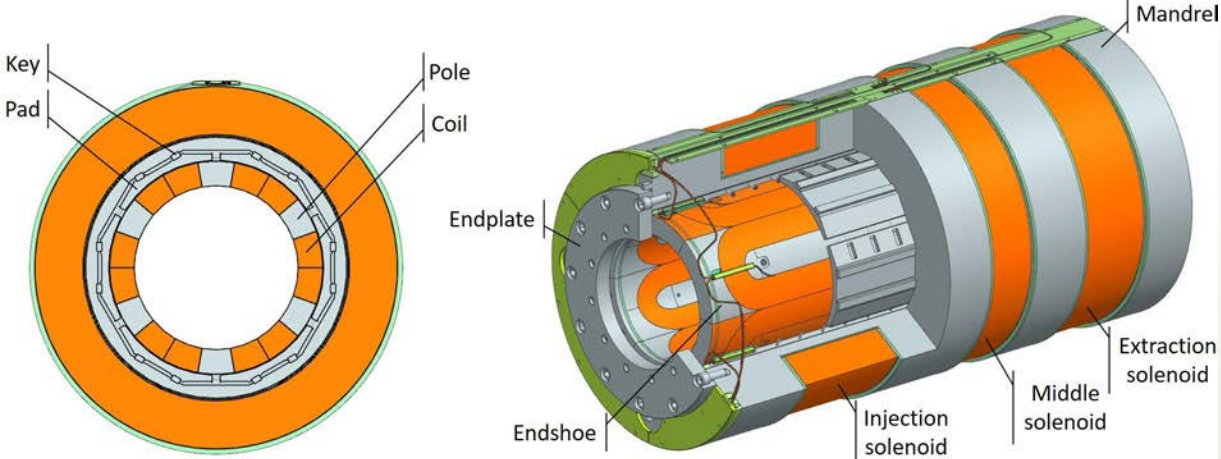
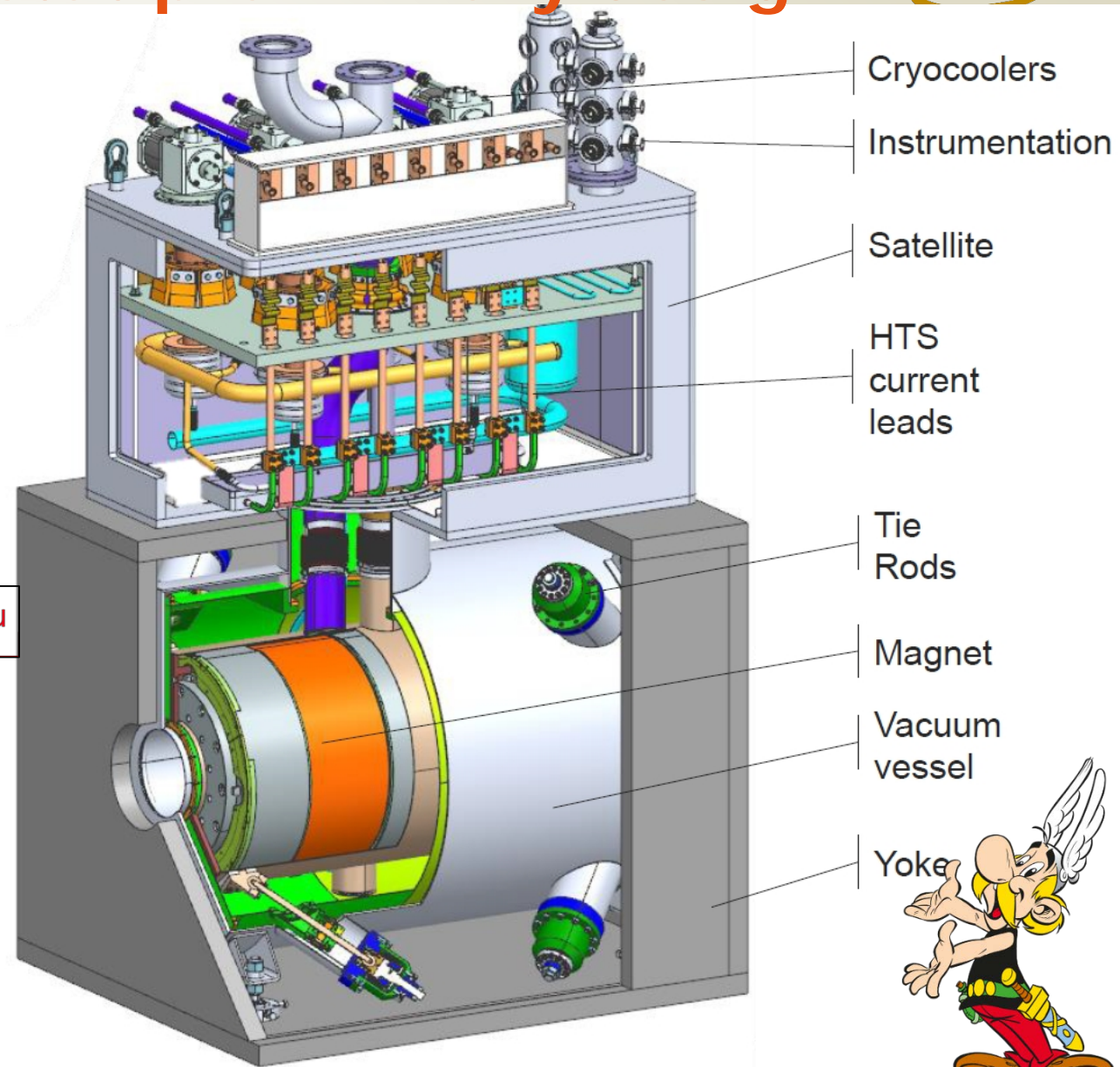
- Magnet and cryostat preliminary design done by CEA
- Construction subcontracted to the industry
- Stand alone magnet test planned at CEA before assembly in the cryostat
- 12 racetrack coils built
- 16 km of spare cable ordered





# ASTERICS Magnet and Cryostat preliminary design

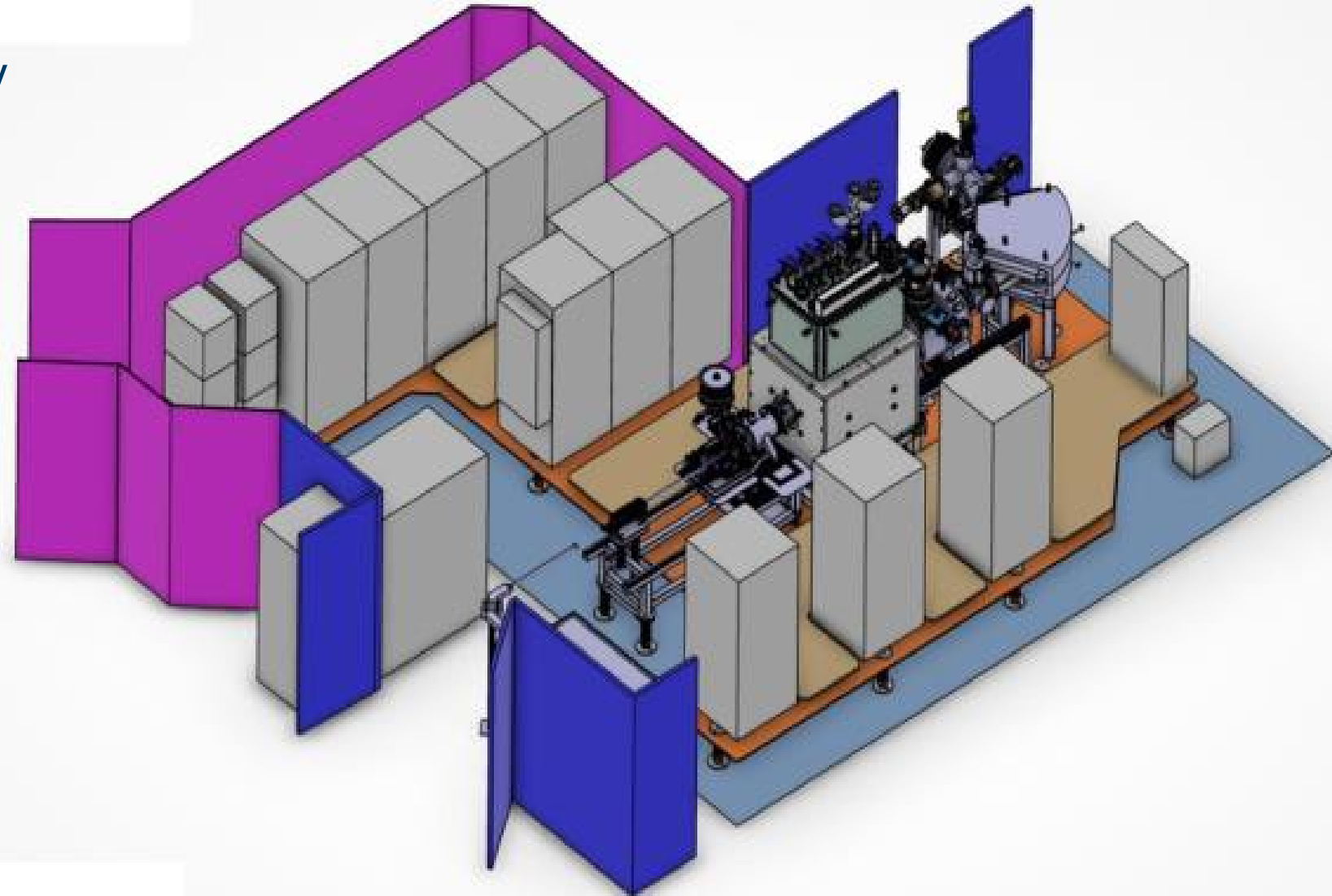
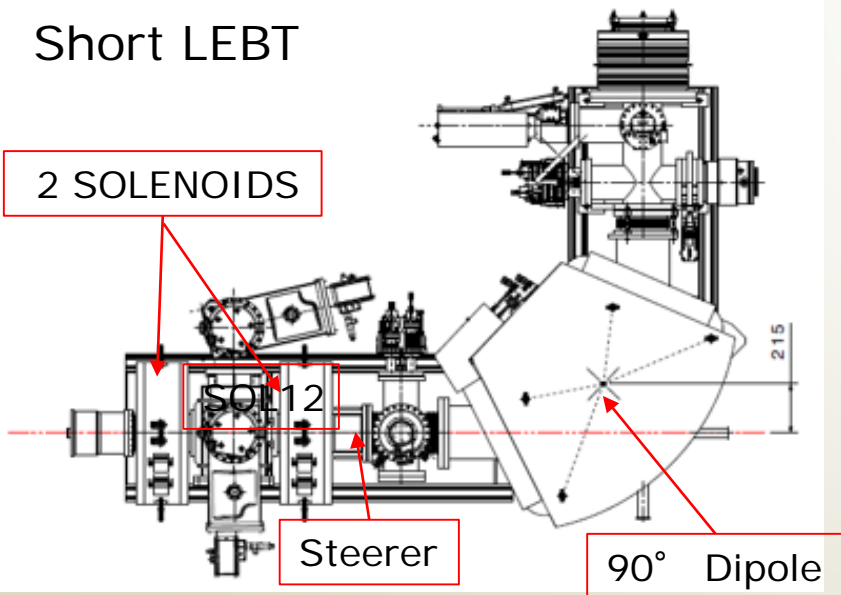
- Bladder and keys technique
- LHe bath, 6 GM-JT crycoolers
- 8 HTS leads
- Redundant instrumentation
- Preliminary design under progress
- Active quench system (to dump coils energy in ext. resistors)



# Source and platform preliminary design (under progress)

- 50 KV HV platform
- Source HV tunable: 20-40 kV
- LEBT on platform
- 28 GHz gyrotron @ ground

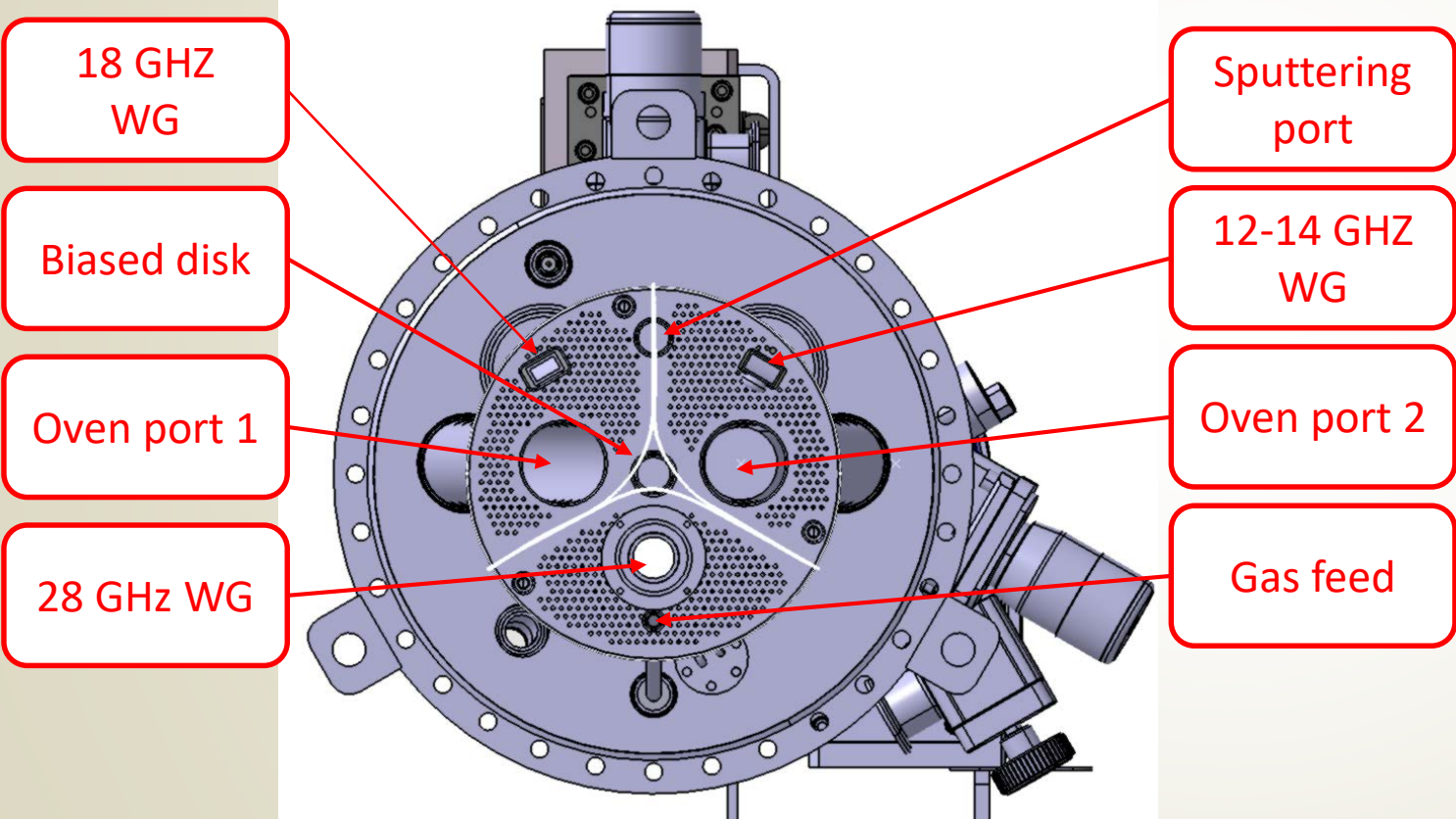
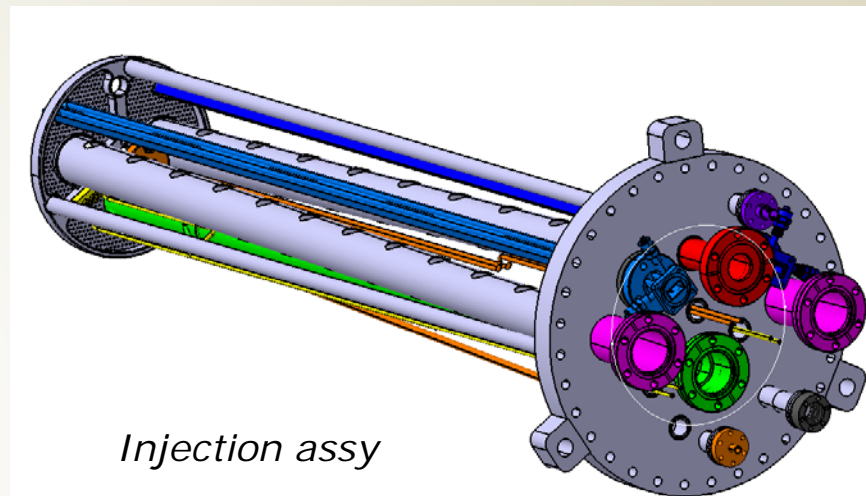
Short LEBT



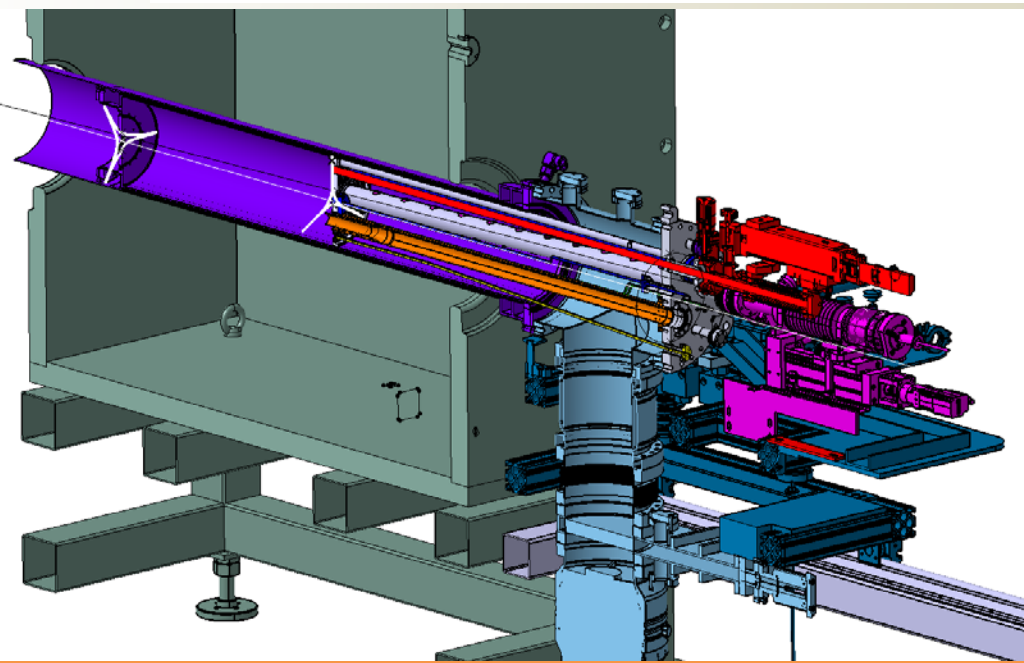


# Source mechanics preliminary design

- The large chamber diameter allows to pass many feedthroughs

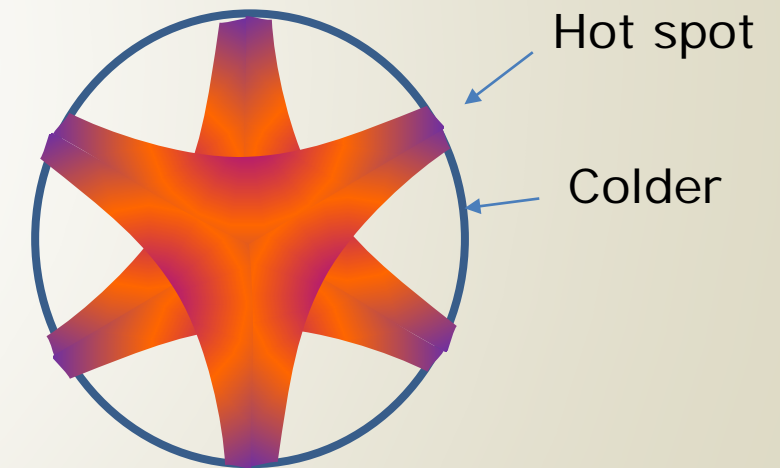
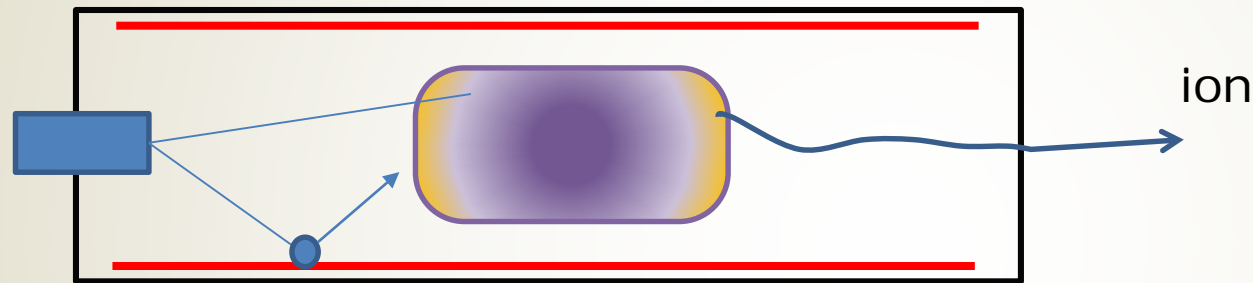


ASTERICS Injection assy preliminary design



# Motivation to develop a new generation of ECRIS hot liners

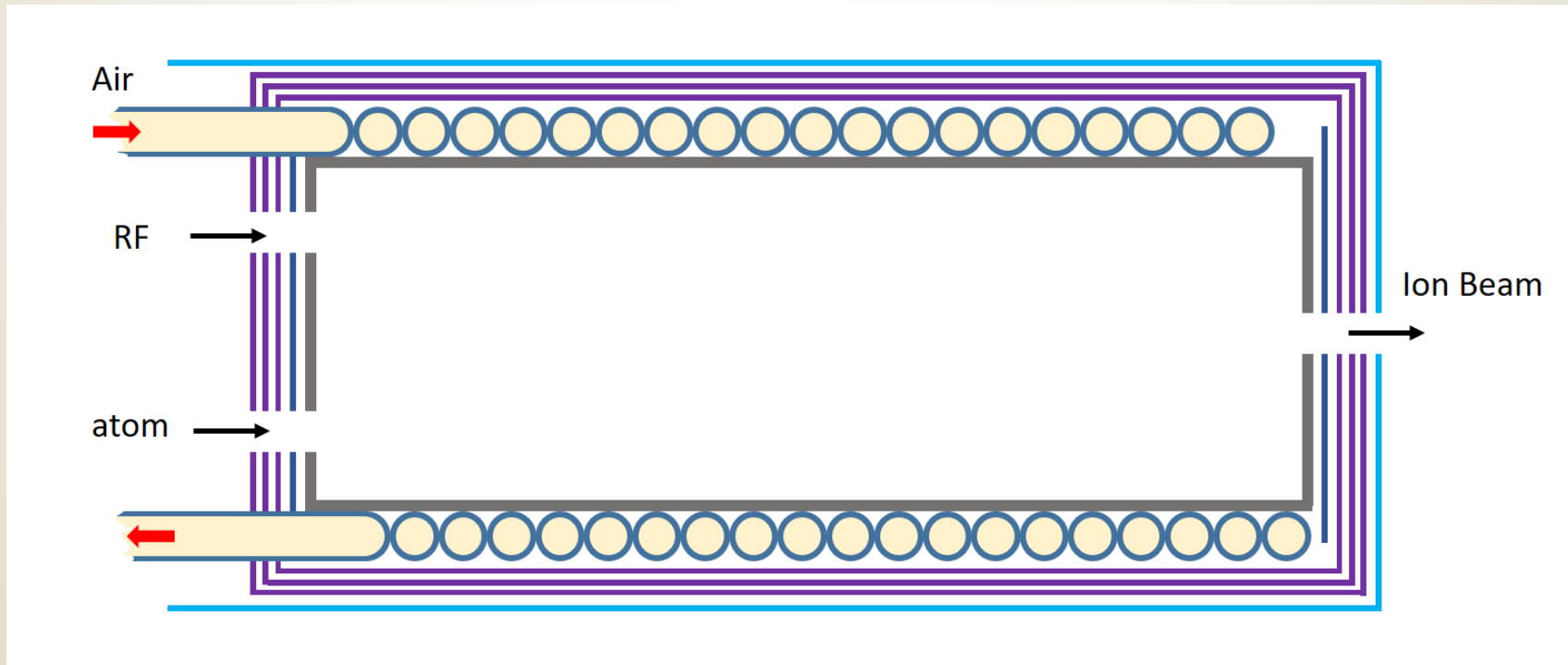
- Liner used to enhance the production yield of high vapor pressure metal beams like Ca
- Today hot liners in ECRIS are usually thin foils (~0.1 mm) directly heated by the plasma



- No control of the liner temperature and evaporation rate
- Thin liner => poor thermal conduction in the liner  
=> hot spots => easy to melt
- If RF power is OFF while oven is ON => accumulation of metals on the liner  
=> overshoot of metal vapor when RF is resumed

# Concept of thick active liner for ECRIS

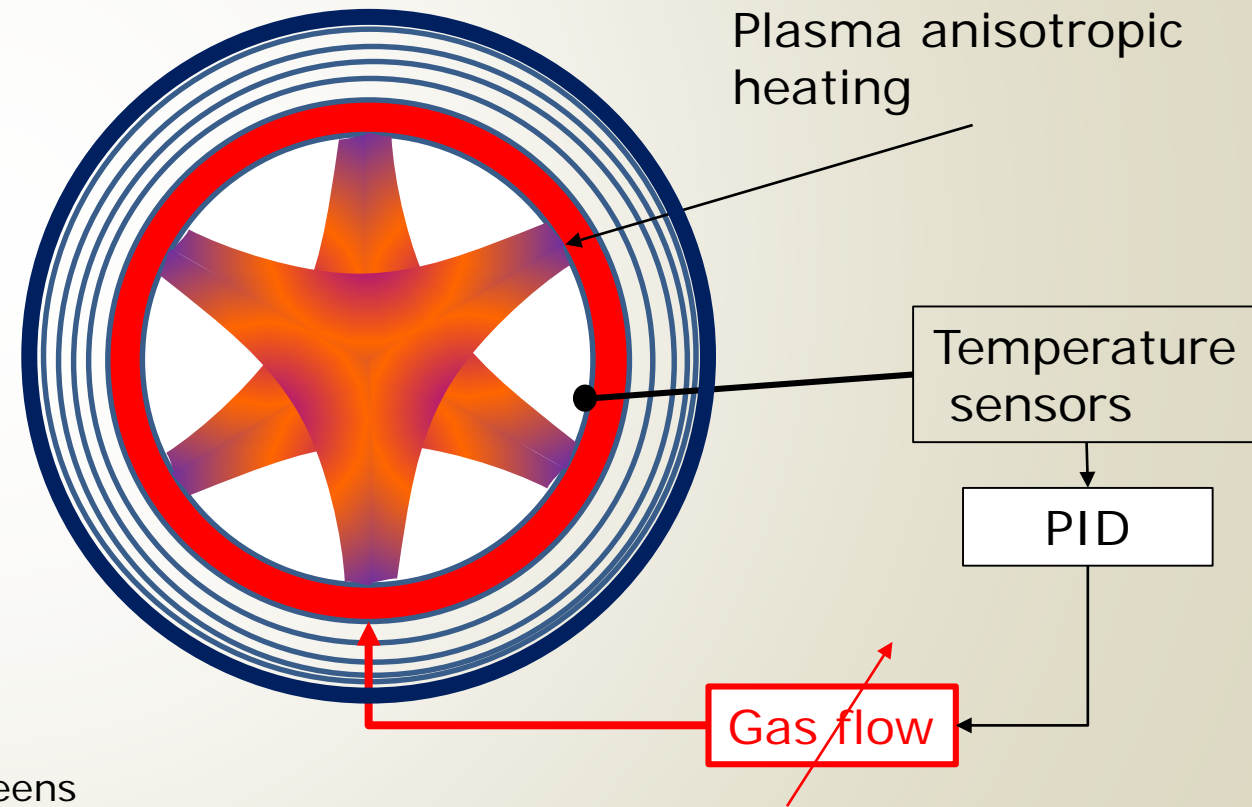
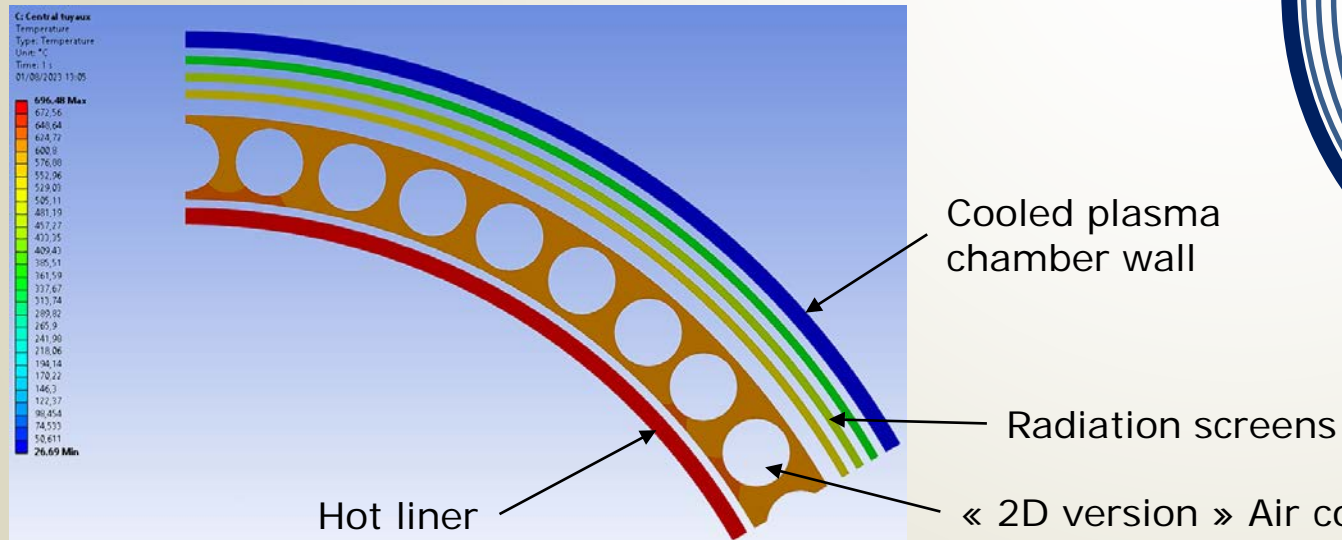
- Use a thick hot liner to homogenize its temperature
- Add radiation screens to increase the mean liner temperature
- Add a stainless steel helically wrapped tube in which compressed air can flow, acting as a radiation screen
- The air flow reduces the liner temperature





# Active hot liner simulation

- Thermal Simulation with Ansys 2D
- Anisotropic power flux
- Air forced convection and thermal radiation modelled
- radiation screens
- 0 or 12 m<sup>3</sup>/h airflow
- Center of plasma chamber (6 loss lines)
- Edge of plasma chamber (3 loss lines)



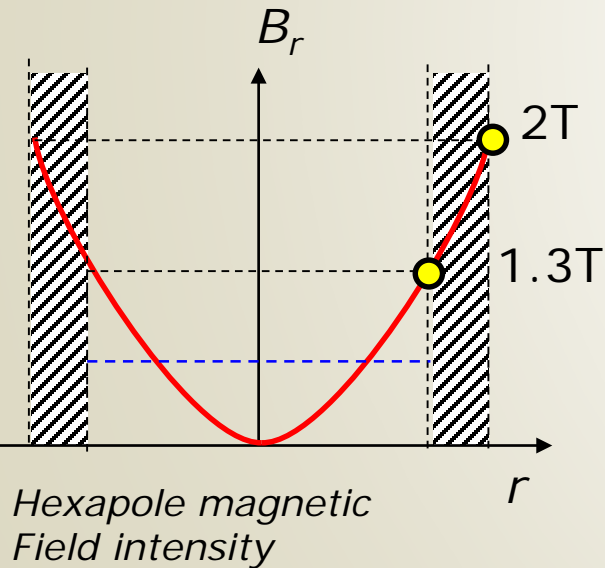
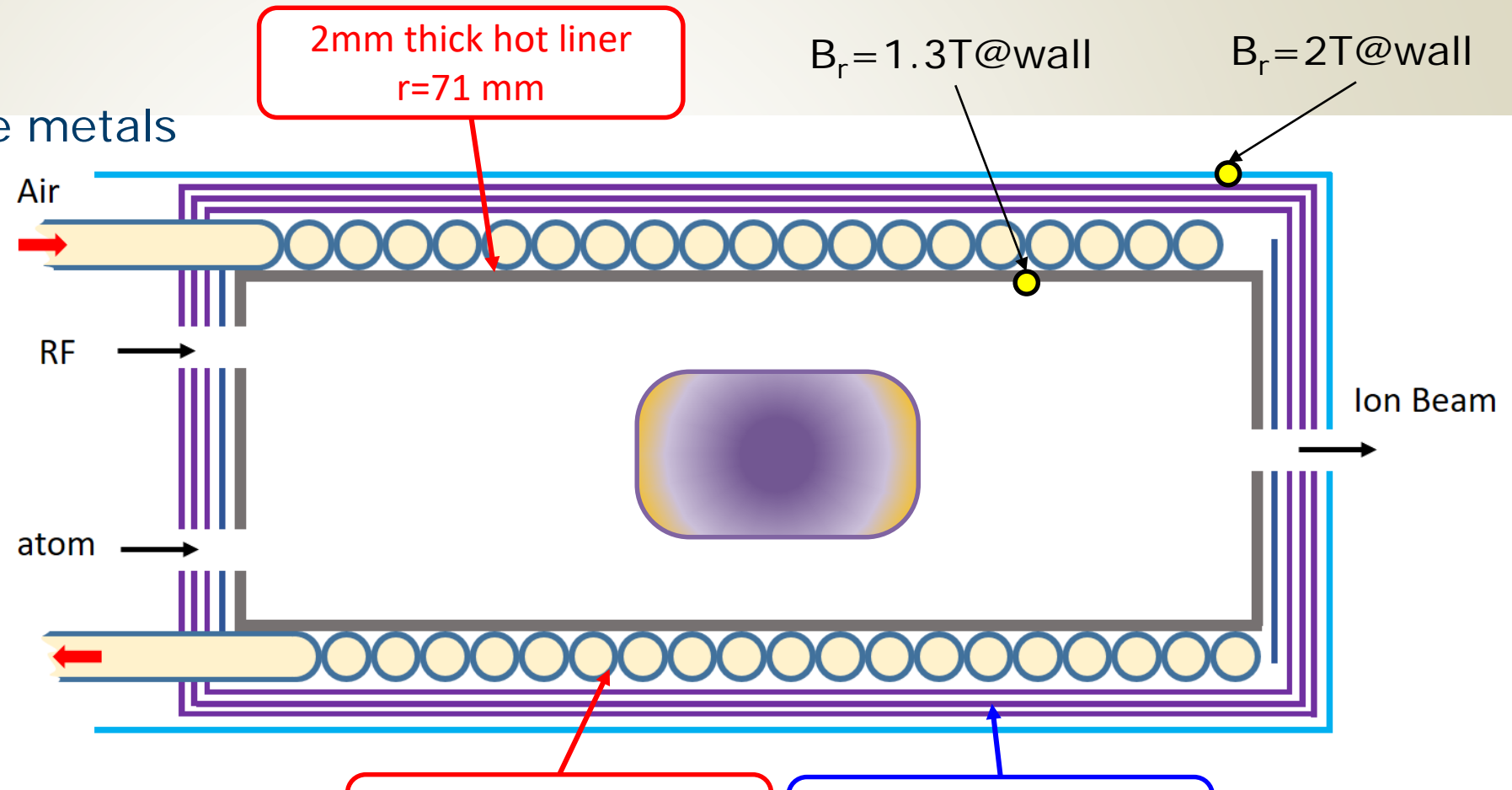


# Simulation results and discussion

- Max reachable temperature with 2 kW RF is 800° C with 3 screens
- Max temperature with 2 kW RF is 700° C without screens
- Thick liner wall => temperature homogeneity at wall +/- 12° C
- Air cooling can **remove 200° C** for a 12 m<sup>3</sup>/h air flow => partial control of the evaporation
  
- The temperature range of liner operation can be adapted by changing the number of screens
- The Air cooling allows to keep the liner temperature constant while changing other source parameters (gas glow, RF)
- The Air cooling helps to mitigate overshoots of evaporation after a RF shutdown

# A thick active hot liner for ASTERICS

- $\leq 20$  mm radial thickness ( $R=91$  to  $R=71$  mm)
- For 18 GHz RF heating
- For high vapor Pressure metals



$B_{ECR}=0.64 T$





THANK YOU FOR YOUR ATTENTION



Any question?

