

HAICU-UBC Development Progress Report

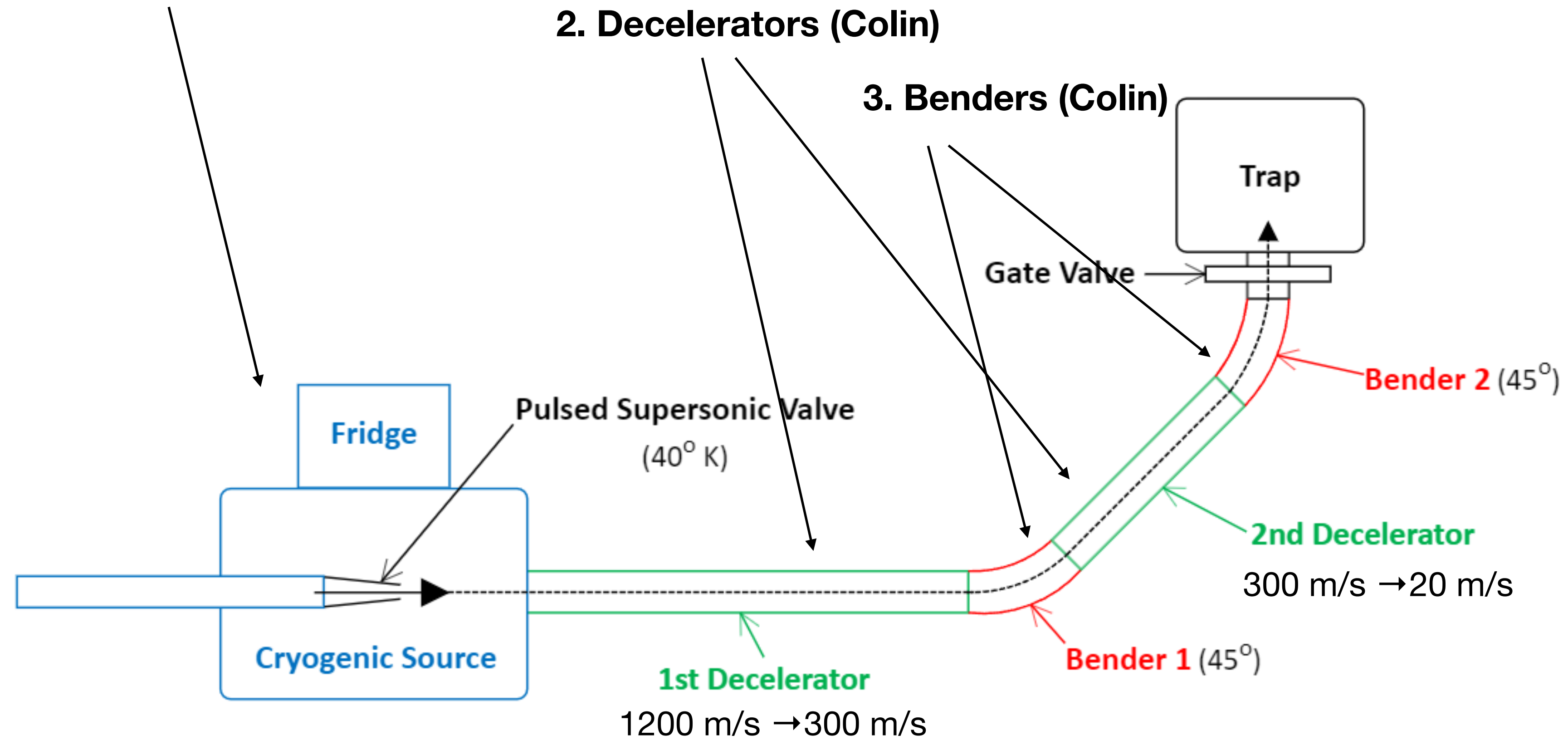
Dec 22, 2023

Reza, Colin, Tony, Taka

OVERVIEW

1. H source (Reza)

5. H Detection via LyA (Reza)



4. Control Electronics (Tony)

OVERVIEW

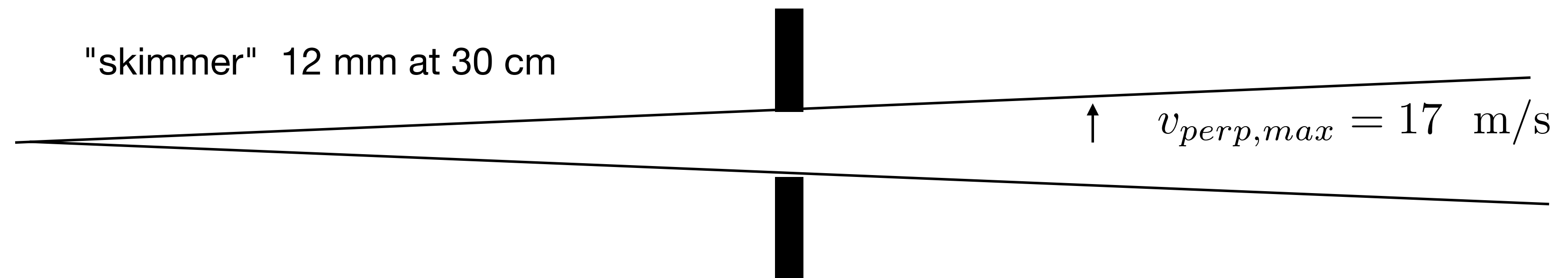
1. H Source

Pure H₂ or H₂ in Ne or He supersonic expansion

Supersonic beam	30 % H ₂ in Ne at 100 K, 10 bar : 830 m/s ± 15 m/s	H ₂ density	2×10^{13} /cc
	30 % H ₂ in He at 30 K, 10 bar : 670 m/s ± 10 m/s	H ₂ density	6×10^{13} /cc

$$v_{axial} < 20 \text{ m/s}$$

Pulsed gas valve (20 - 100 us opening) : beam length 2 - 8 cm at 800 m/s



H generation: plate discharge at >2.5 kV



H density (target) 1×10^{12} /cc

Supersonic beam

1 st Mach disk

Adiabatic expansion: conservation of total enthalpy

directed mass flow maximum velocity

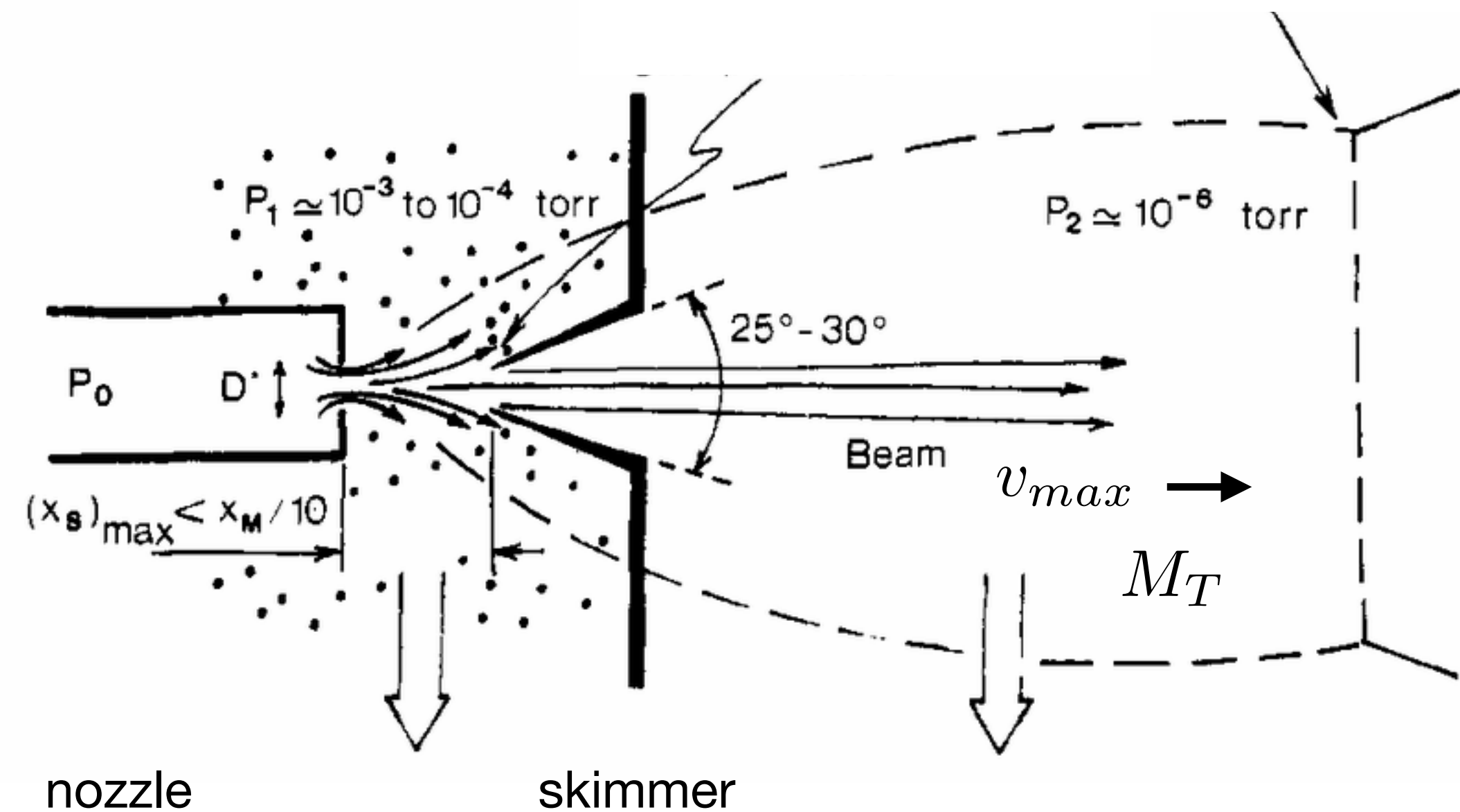
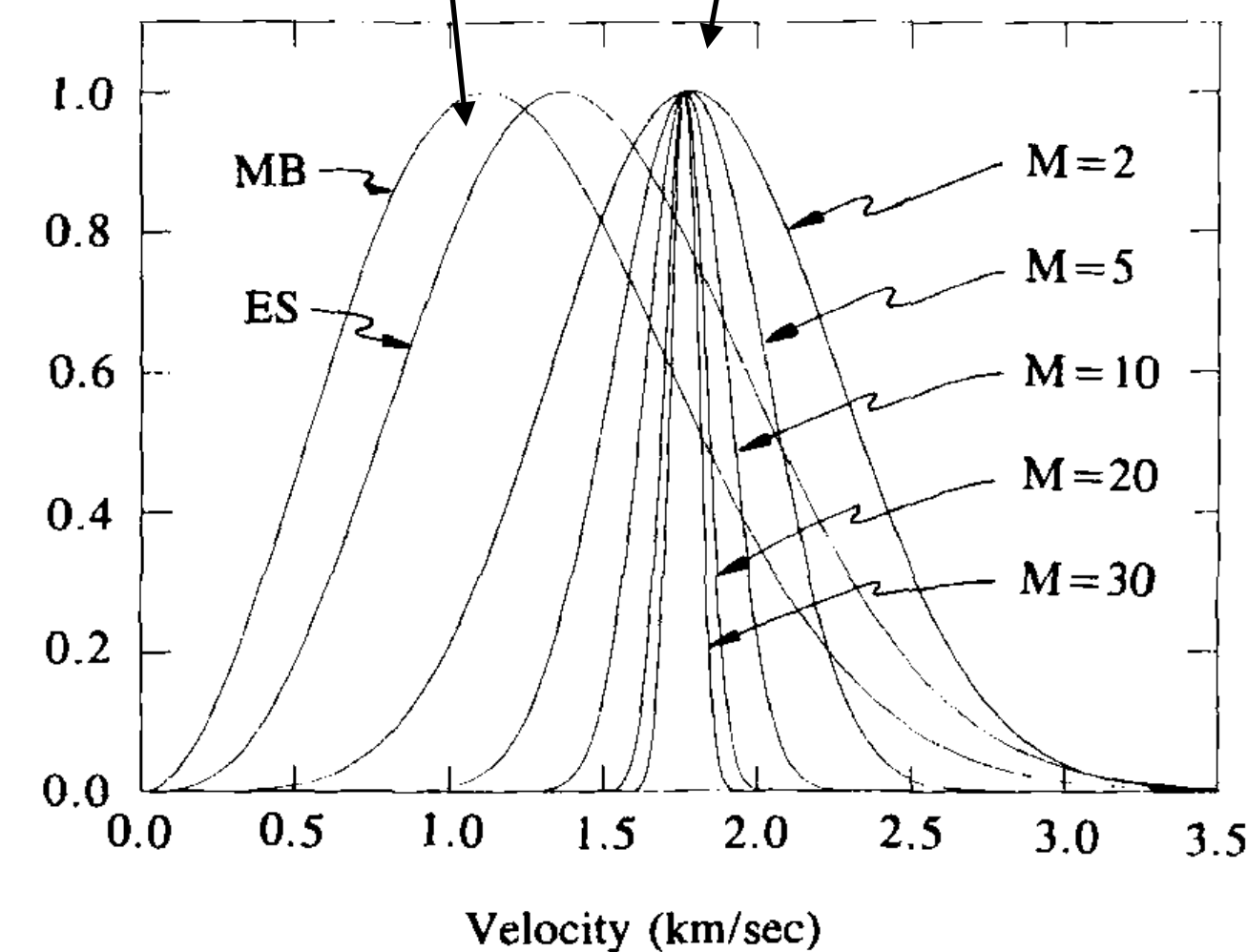
$$v_{max} = \sqrt{\frac{2H(T_0)}{m}} = \sqrt{\frac{2C_p T_0}{m}}$$

$$\frac{T(x)}{T_0} = W^{-1} \quad \frac{\rho(x)}{\rho_0} = W^{-\frac{1}{\gamma-1}}$$

$$W = 1 + \frac{\gamma-1}{2} M(x)^2$$

Thermal beam

supersonic beam



Mach number

$$M(x) = \frac{v(x)}{a(x)}$$

Speed of sound

$$a(T) = \sqrt{\frac{\gamma RT}{m}}$$

Terminal Mach number

$$M_T = G(\sqrt{2}\sigma\rho_0 D\epsilon)^{\frac{\gamma-1}{\gamma}}$$

σ effective cross section

γ heat capacity ratio

D nozzle orifice diameter

ρ_0 stagnation density

ϵ collision efficiency $\epsilon \leq 1$

G constant

	sound velocity at the nozzle m/s	max velocity m/s	skimmer Mach number	skimmer temp/K	skimmer density /m ³	skimmer velocity deviation ~ sqrt(kT/2m) m/s
300 K, 2bar						
He	1019.13	1765.19	394.91	5.77E-03	4.13E+18	2.45
Ne	453.91	786.20	394.91	5.77E-03	4.13E+18	1.09
H2	1316.23	2943.17	64.85	3.56E-01	2.38E+18	27.11
100K, 10 bar						
30% H2 in Ne		827.51		3.70E-02	1.66E+18	18.97

Reza

H Source Summary

Scope

- Generate H beam with $> 10^{12}$ particles/cc at < 900 m/s velocity

Progress

- Confirmed that He and Ne gas discharges would work for H generation.
- Optimization is still underway. Limited cooling test due to the size of the current test chamber.

Outlook

- Refrigerated large source chamber ready to test January 2024.
- Test of higher voltage discharge in January 2023
- Finalize the nozzle condition by February.

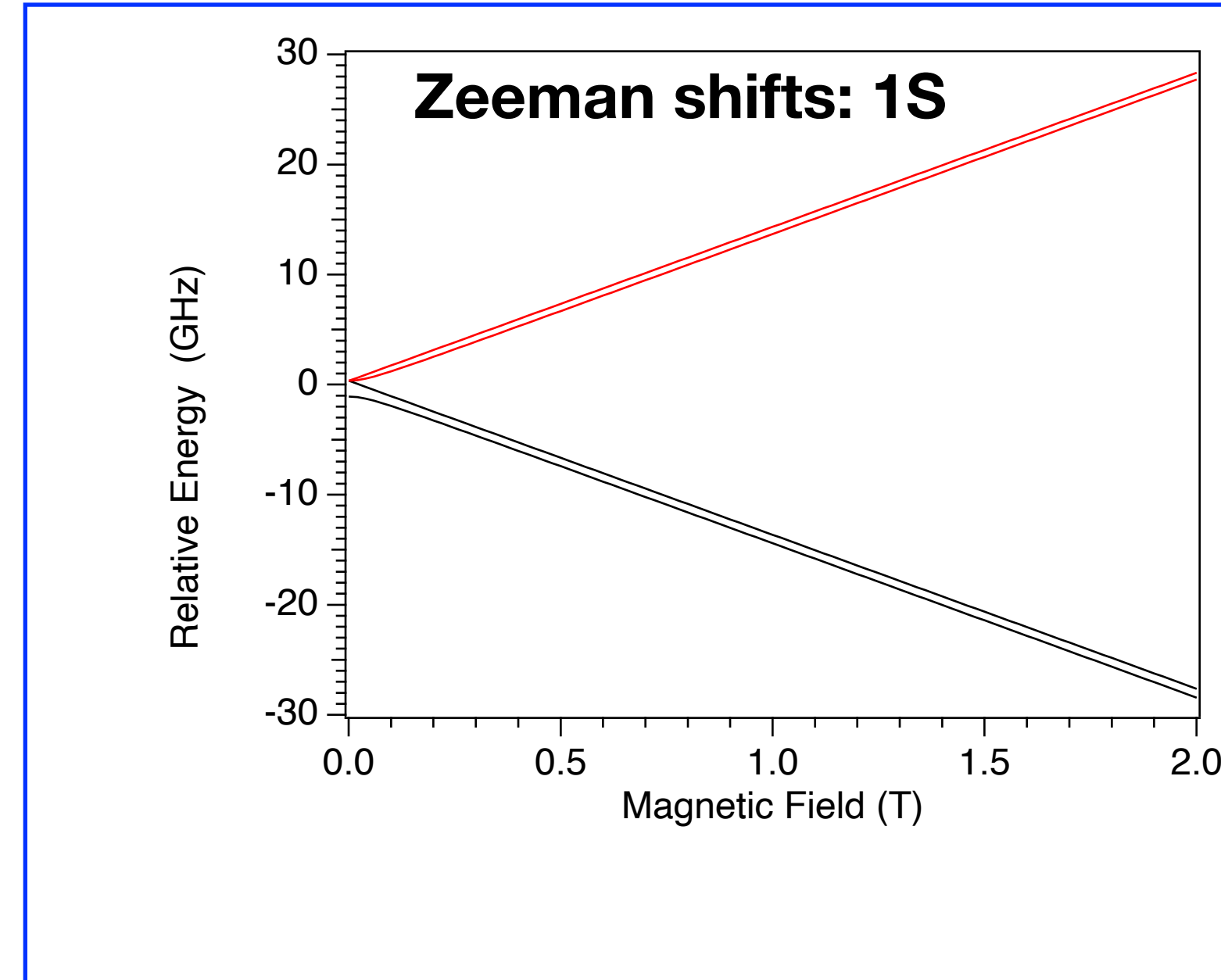
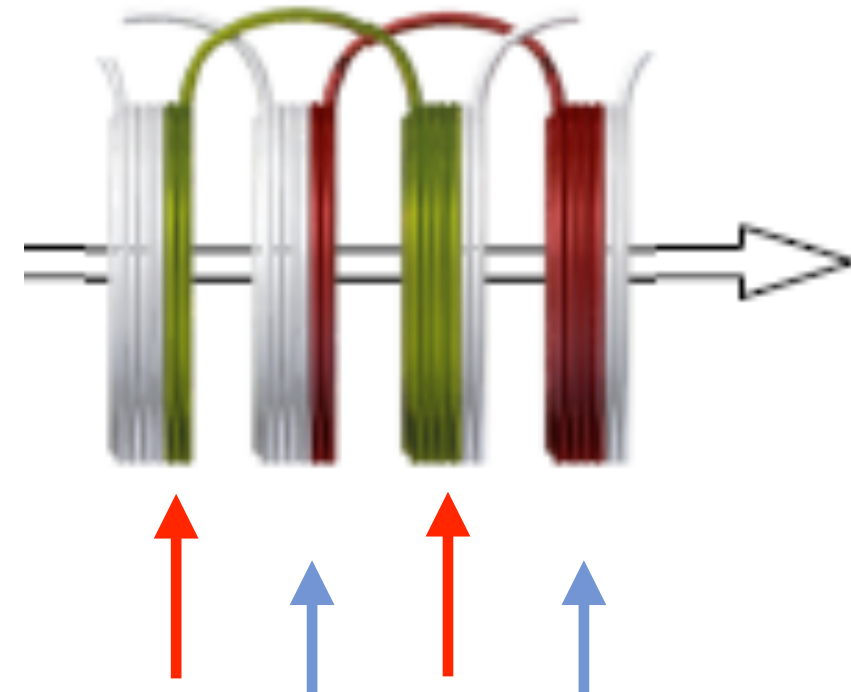
Risks

- Optimization is still underway. Difficult to predict final achievable density.
- Long term stability of the discharge nozzle is unknown
- Need to improve laser frequency stability and calibration.

OVERVIEW

2. Decelerator

Moving trap decelerator

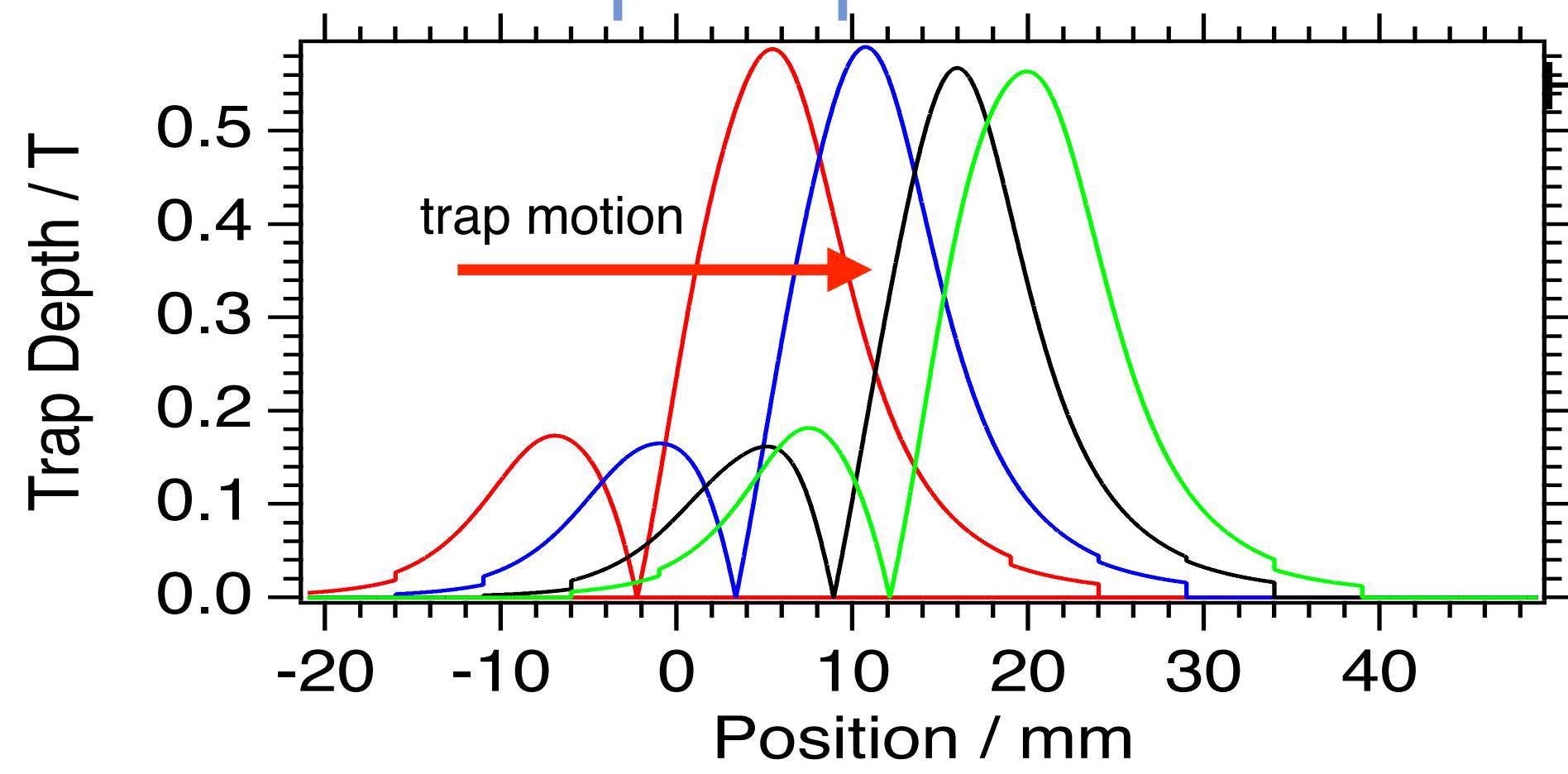


$$\frac{dE}{dB} = g_e \mu_B M_s \sim \mu_B \sim 0.466 \text{ cm}^{-1} / \text{T}$$

Force

$$F = -\frac{dE}{dz} = -\frac{dE}{dB} \frac{dB}{dz}$$

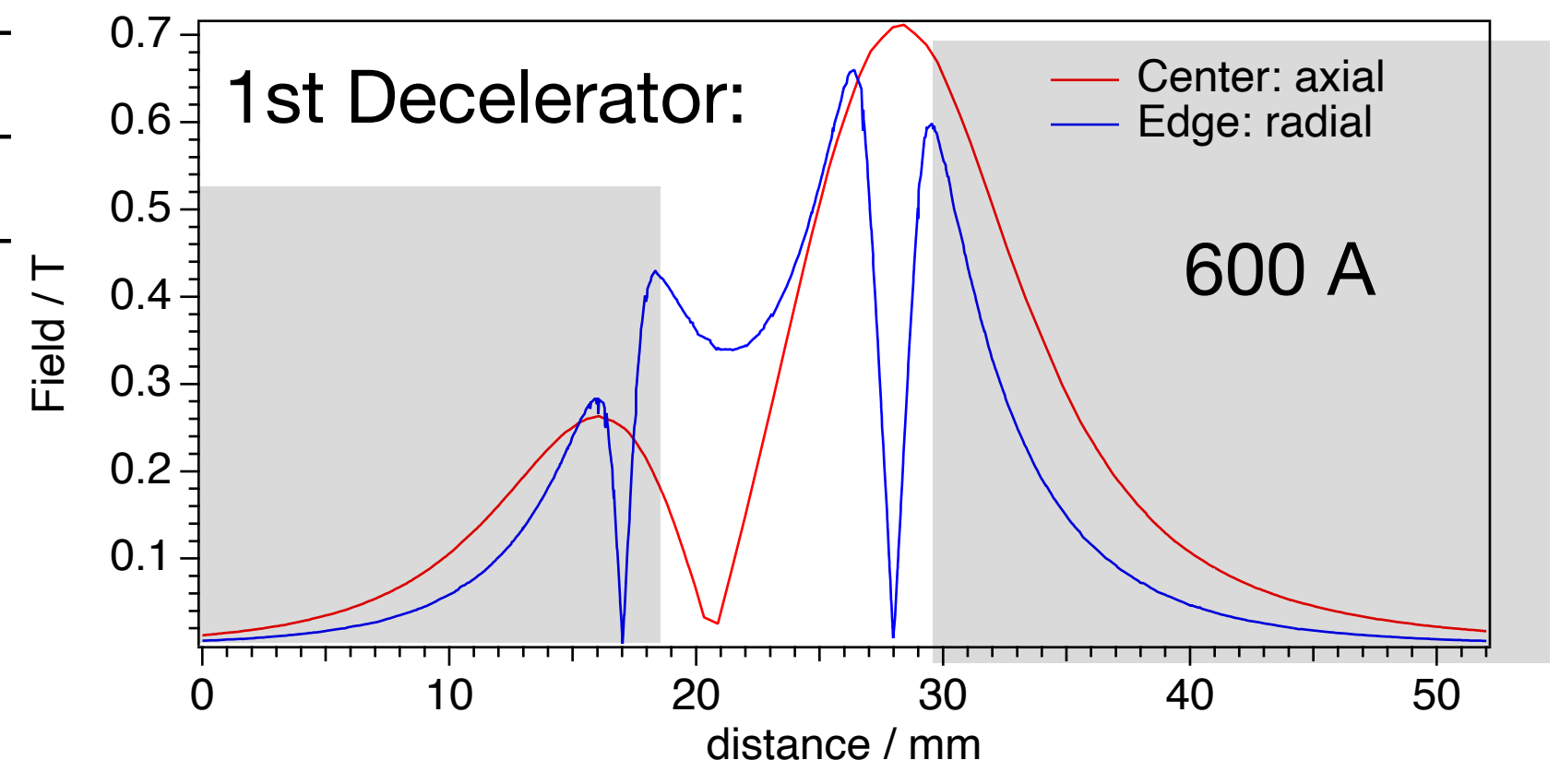
$$\frac{dB}{dz} \sim 100 \sim 170 \text{ T/m}$$



HAICU design

1st Decelerator: 12 mm diameter, 2 * 4 and 4 * 4, 24 AWG
 2nd Decelerator: 10 mm diameter, 2 * 4 and 4 * 4, 26 AWG

trap volume ~ 0.1 cc



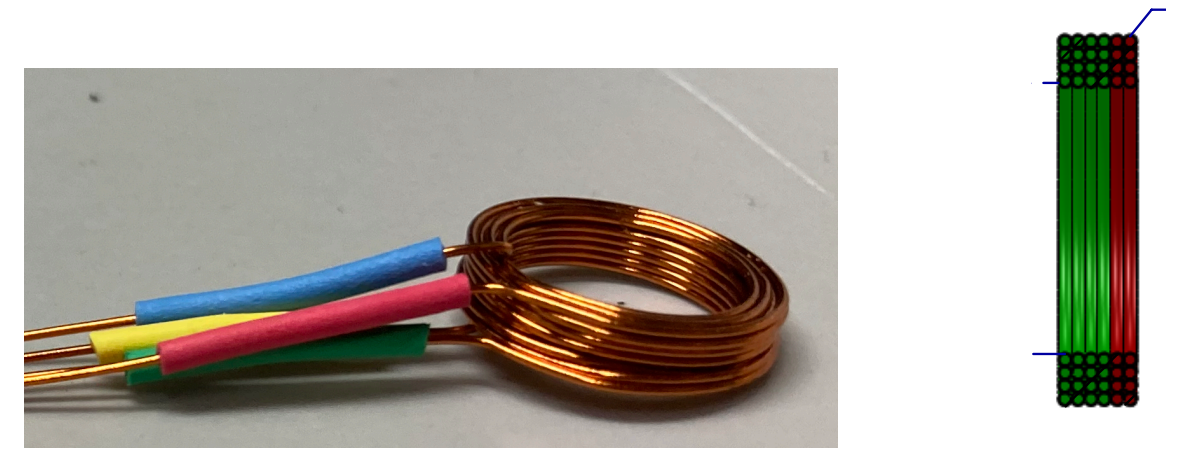
Trap condition

$$v_{axial,max} = 46 \text{ m/s}$$

$$v_{radial,max} = 61 \text{ m/s}$$

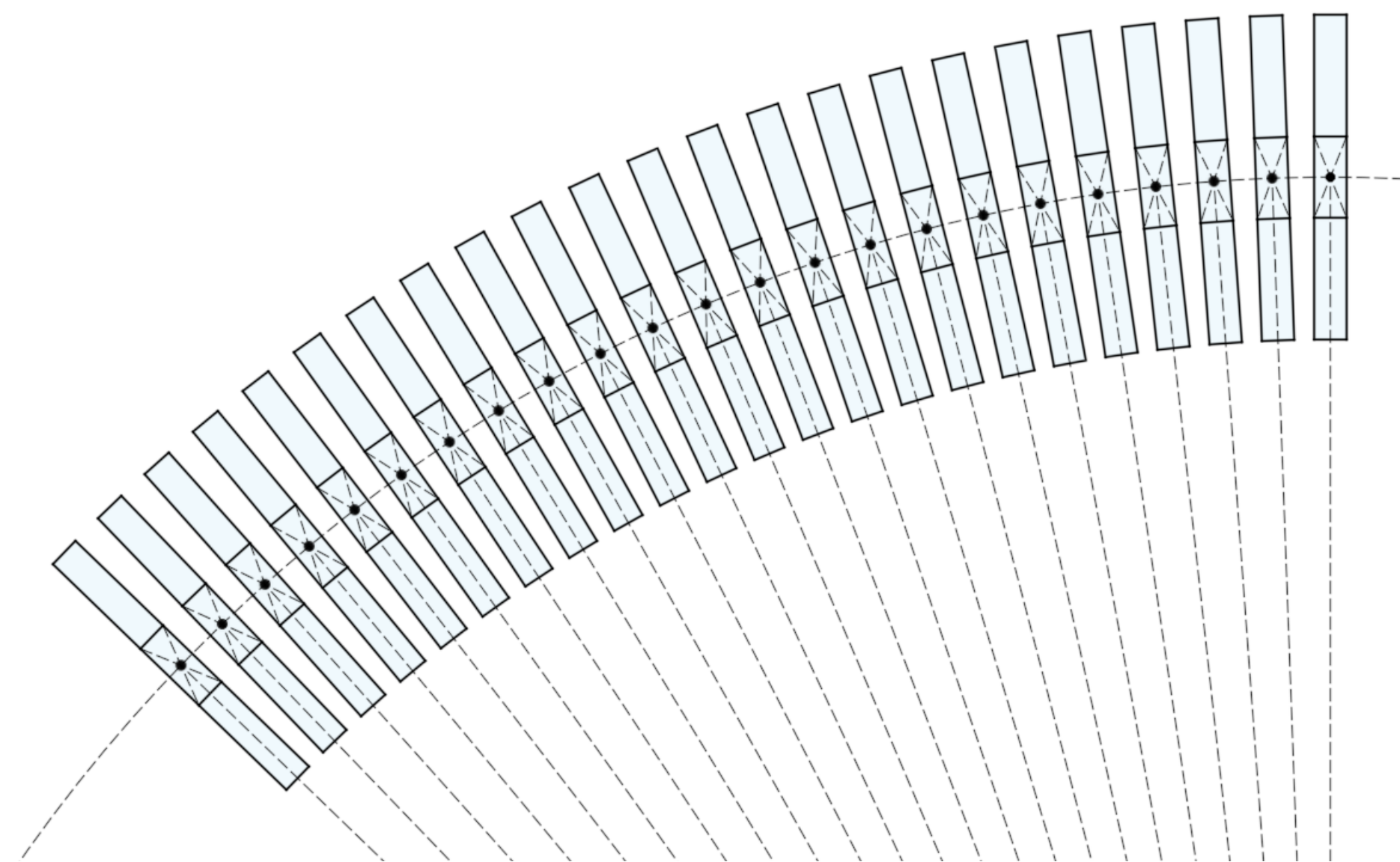
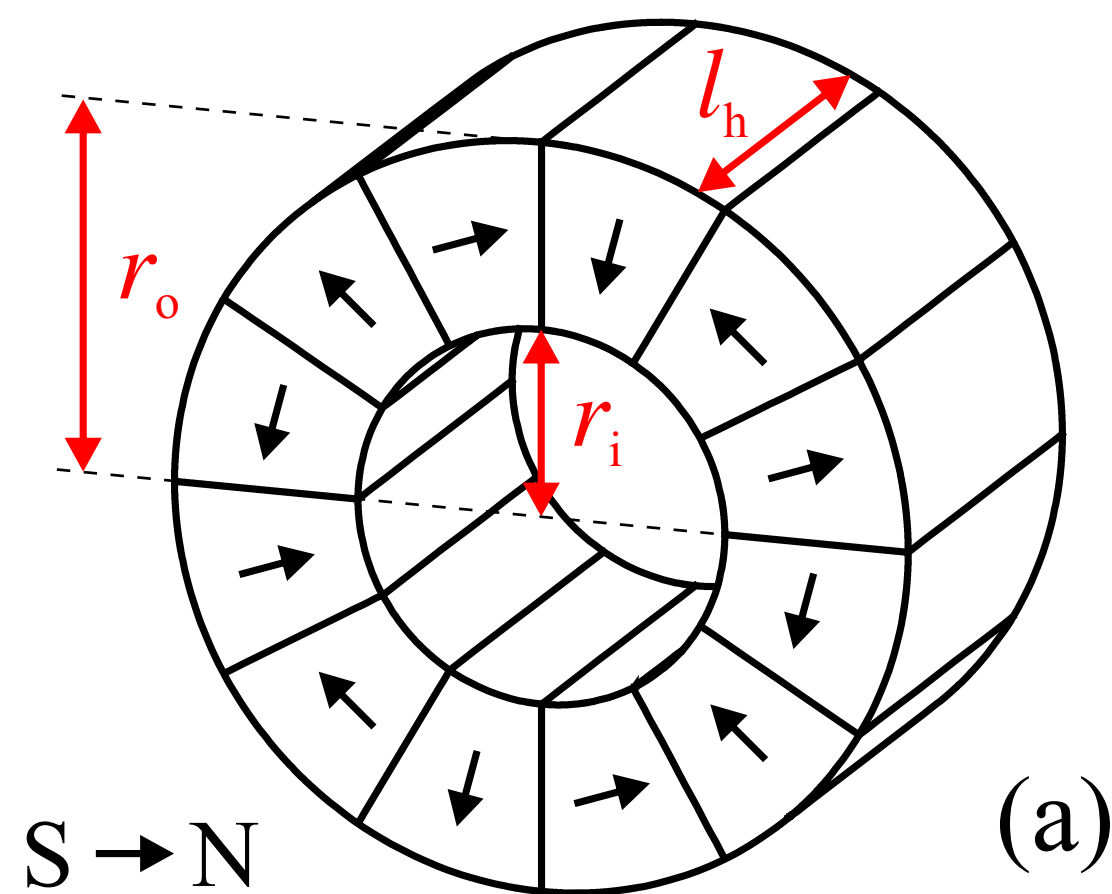
Deceleration efficiency

10 - 100 %



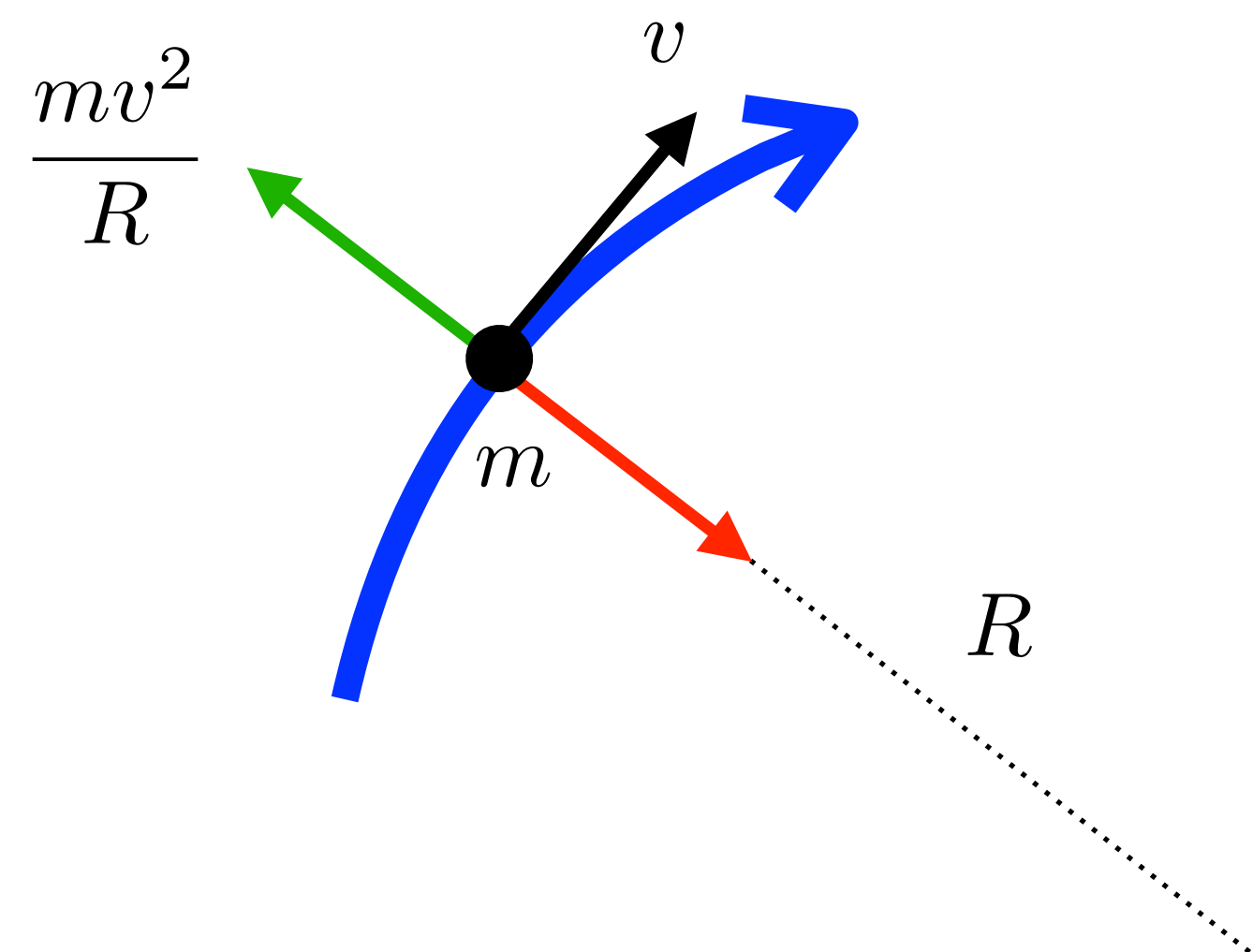
OVERVIEW

3. Bender 1 Halbach array permanent magnets



centripetal force $= \frac{mv^2}{R}$

transverse magnetic force $= -\frac{dE}{dR} = -\frac{dE}{dB} \frac{dB}{dR} \sim -g_e \mu_B M_s \frac{dB}{dR} \sim \mu_B \frac{dB}{dR}$



$$\frac{mv^2}{R} = \mu_B \frac{dB}{dR}$$

Maximum velocity

$$v = \sqrt{\mu_B \frac{R}{m} \frac{dB}{dR}} = 74.7 \sqrt{R \frac{dB}{dR}}$$

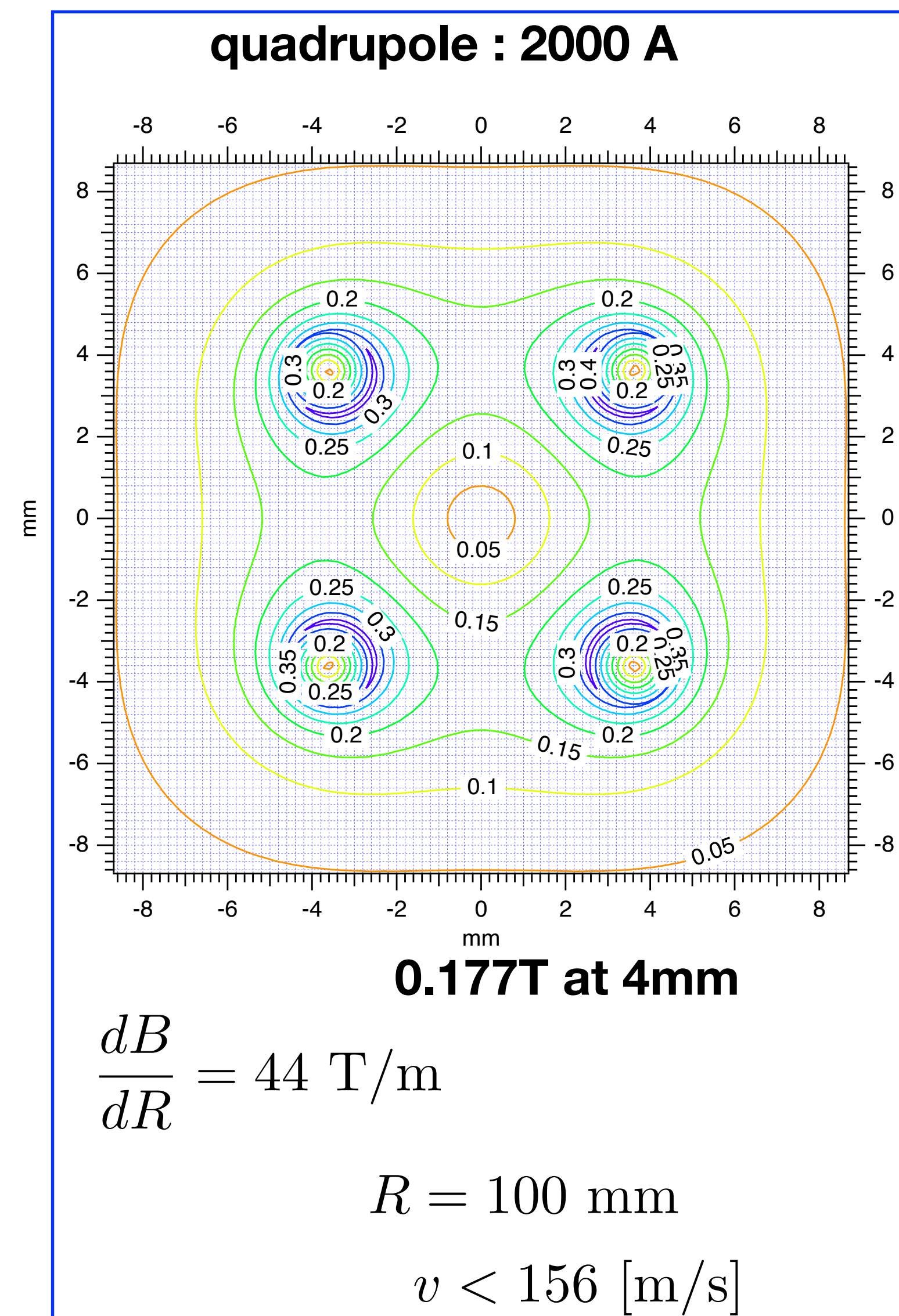
for $m = 1$

$$\frac{dB}{dR} \geq 110 \text{ T/m} \quad v < 360 \text{ [m/s]} \quad \text{at} \quad R = 200 \text{ mm}$$

OVERVIEW

3. Bender 2

quadrupole



Colin

Decelerator and Bender Summary

Scope

- The 1st decelerator 900 m/s → 350 m/s, and the 2nd decelerator 350 m/s → 20 m/s.

Progress

- Finalized the decelerator and the bender design. Confirmed that the trap moves smoothly.
- Ordered all necessary electrical components. Mechanical design almost completed

Outlook

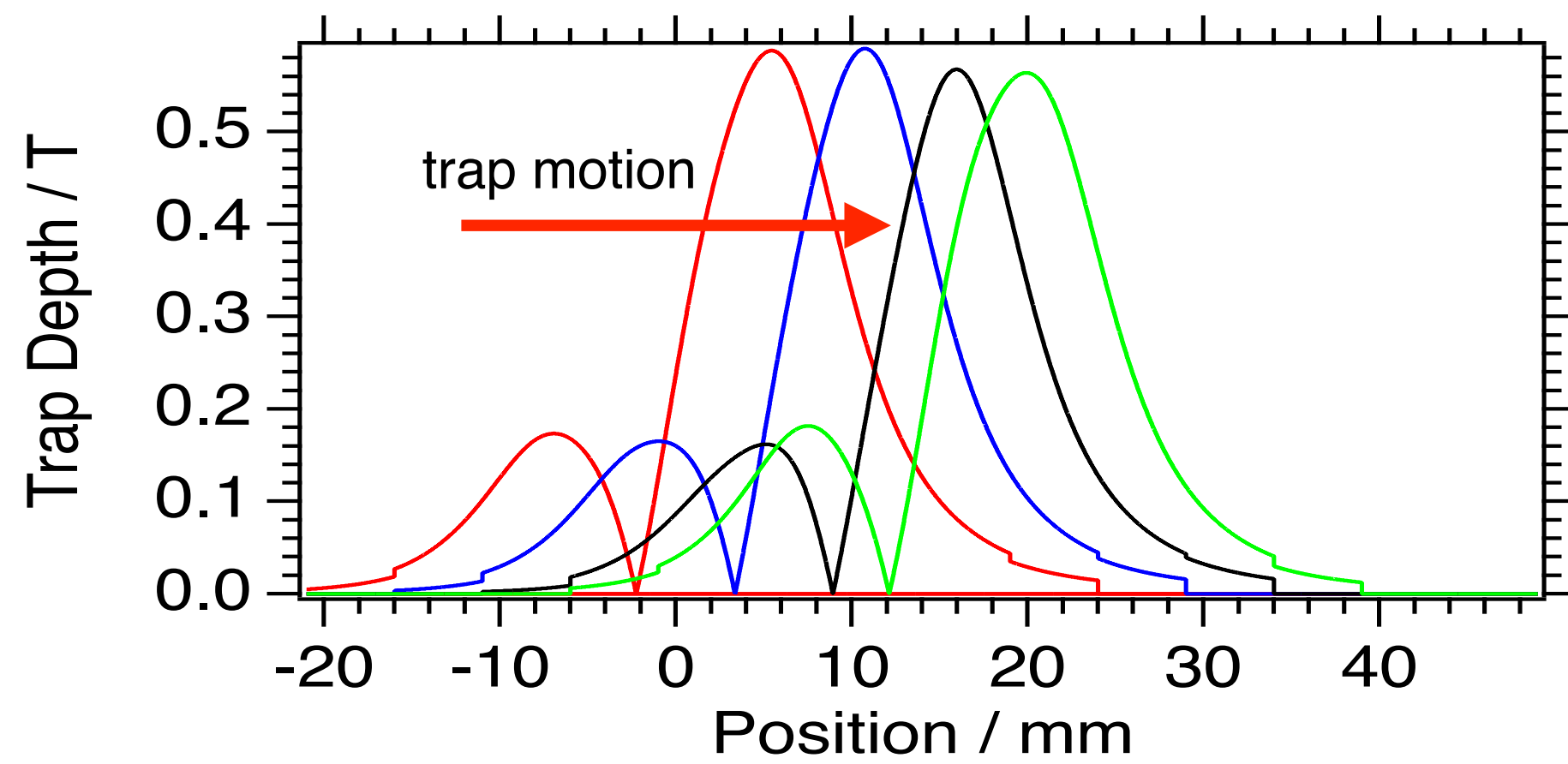
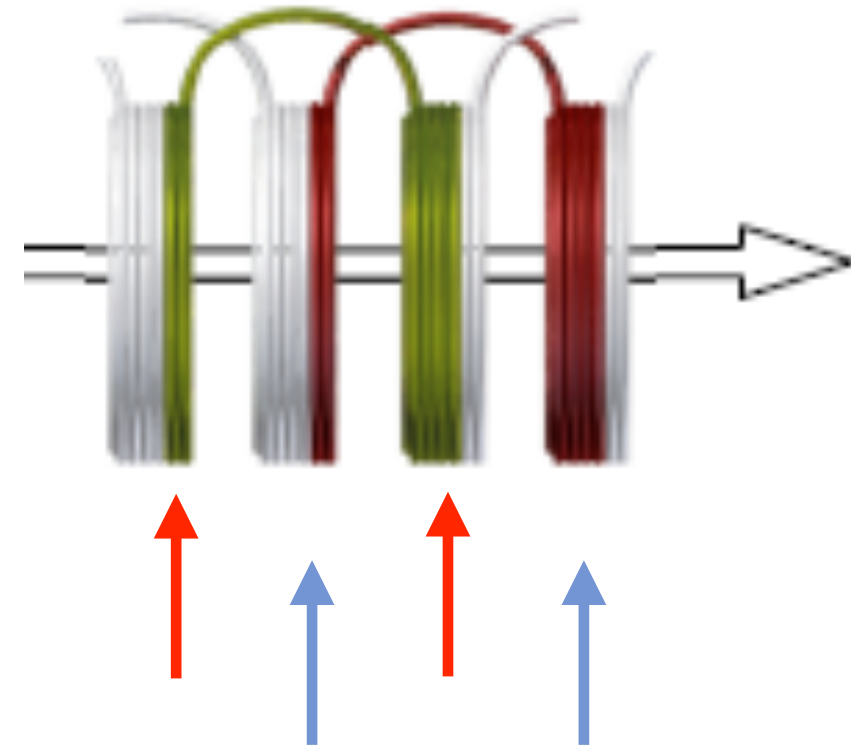
- Finalize the mechanical design by January. Installation of all mechanical components in February.
- Install and assemble all electrical components in February.
- Deceleration test in early March. Optimization during the summer.
- Benders will be tested in January (with CH3)

Risks

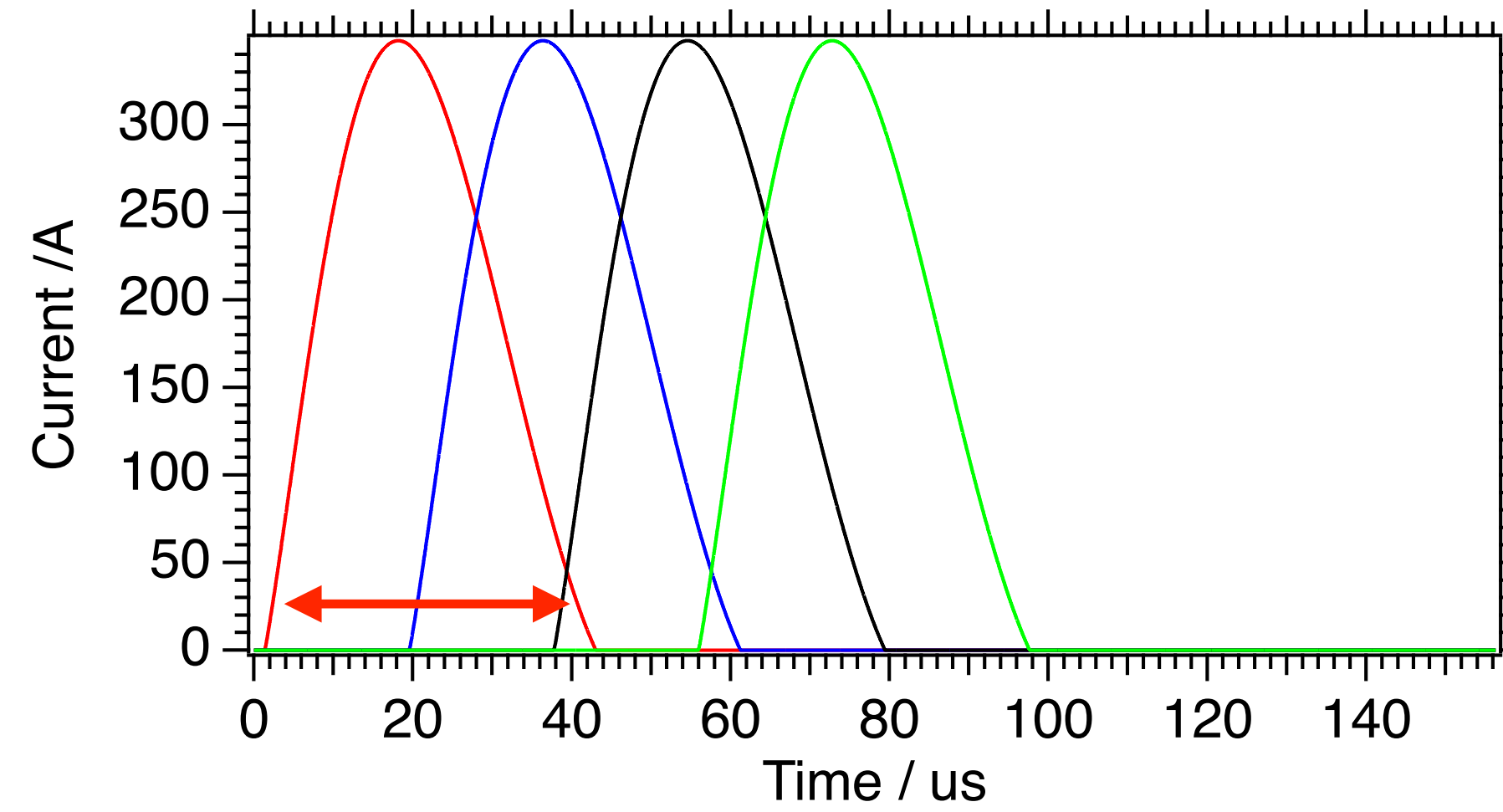
- No design risk.
- A lot of man power will be needed in February for assembly.
- The bender performance is not well characterized (until January).

OVERVIEW

4. Control Electronics



5 - 250 us π pulse current



Initial: 1000m/s = 10 us pulse (5 us rise)
Final: 50 m/s (150 mK)= 200 us pulse

Tony

Electronics and System Control Summary

Scope

- 32 TuneBox Sets are required for 900 m/s (each Tunebox drives every 32nd trap).
- 4 banks of discharge boards are needed to provide 32 busbar paths along the decelerator
- 4 FPGA based MLDs (72 output high speed digital pattern generators) drive tuneboxes and discharge boards.

Progress

- The 1st generation system is running in Momose Lab.
- Parts for the 2nd generation are on order. TRIUMF group is migrating current FPGA firmware and PC Side code to Ethernet (currently using USB).

Outlook

- Assembled and ready to test by March.

Risks

- FPGA firmware and PC software development has no set schedule or dedicated resources in the TRIUMF Electronics Development group.
- Need to request >20% FTE of Bryerton between January and March to obtain the new program by the end of March.
- How to combine with other controls

Summary

Outlook

- Momose group will test the deceleration and trapping during the summer time.

Risks

- Relocation from UBC to TRUMF requires a lots of man power. When can we move our system to TRIUMF? Likely Nov 2024, after the 2024 CERN beam time?